

Surfaces & Friction

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- ▶ **Tribology:**
 science of **contact**, **friction**, **wear** and **lubrication**
*Probably the key of most ancient techniques
 (stone tools, fire, wheel...)
 yet a very recent science: « Tribology » invented in 1956...*
- ▶ Solids are contacting through their **surfaces**, forming
 a **sliding interface**
- ▶ The surfaces' interactions are thus controlling/affecting
 the **friction** (and wear) between solids

▶ Dealing with surfaces...

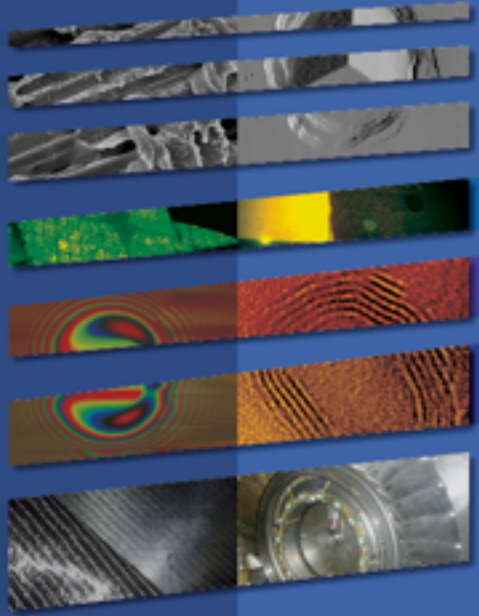
- ▶ What is a « surface »? How to describe it?
- ▶ What are the key properties of a surface?
- ▶ How to characterise a surface?

▶ Influence of surfaces on friction

- ▶ What is « Friction »?
- ▶ How can friction be affected by surfaces?
- ▶ How to study surface-related friction phenomena?

▶ Case-study

- ▶ Solid lubrication processes of Diamond-Like Carbon



Surfaces & Friction

Dealing with surfaces...

Part 1

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What is a surface?

« God created solids, but the devil made their surfaces »

(Gott schuf das Volumen, der Teufel die Oberfläche)

Wolfgang Pauli

***Interface between two phases
(or between a phase and vacuum)***

- ▶ Surface = discontinuity of matter!
- ▶ Describing the solid before considering its surface!
 - ▶ How atoms stay together: chemical bonds
 - ▶ Strongly dependent on the material considered:
metal, ceramic, polymer...
 - ▶ Key-role of the structure of matter at larger scales (nm → μm)

Cohesion of solids

Cohesion of solid: interactions between atoms or molecules

*“Strong” interactions inside molecules or solids,
“Weak” interactions between molecules or solids*

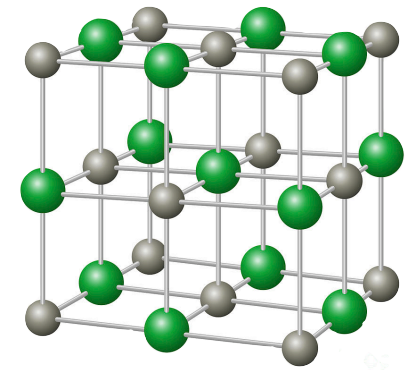
- ▶ **Chemical bonds:** electron charge distributions of the atoms (atomic orbitals) is completely changed
- ▶ **Physical “bonds”:** atoms/molecules remain distinct entities
- ▶ Yet physical binding may be quite strong as well...

Cohesion of solids: chemical bonds

- ▶ **Strong chemical bonds:** atomic interactions through electrons (change in shape and occupation of atomic orbitals)

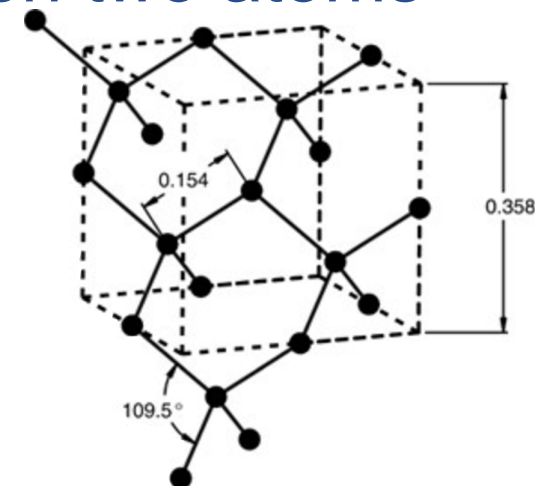
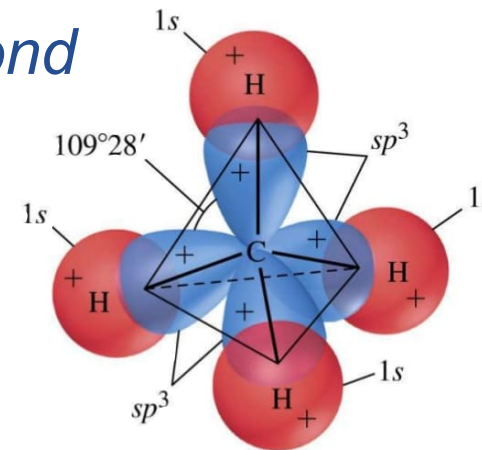
- ▶ **Ionic bond:** exchange of electrons between two atoms

Example: Sodium Chloride (salt!)



- ▶ **Covalent bond:** sharing of electrons between two atoms

Example: Methane CH₄ or Diamond



- ▶ **Metallic bonding:** bonding electrons are delocalised over a lattice of atoms, creating a « gas of electrons »
The behaviour of this gas and its interactions with the lattice controls the metal properties

Cohesion of solids: intermolecular forces

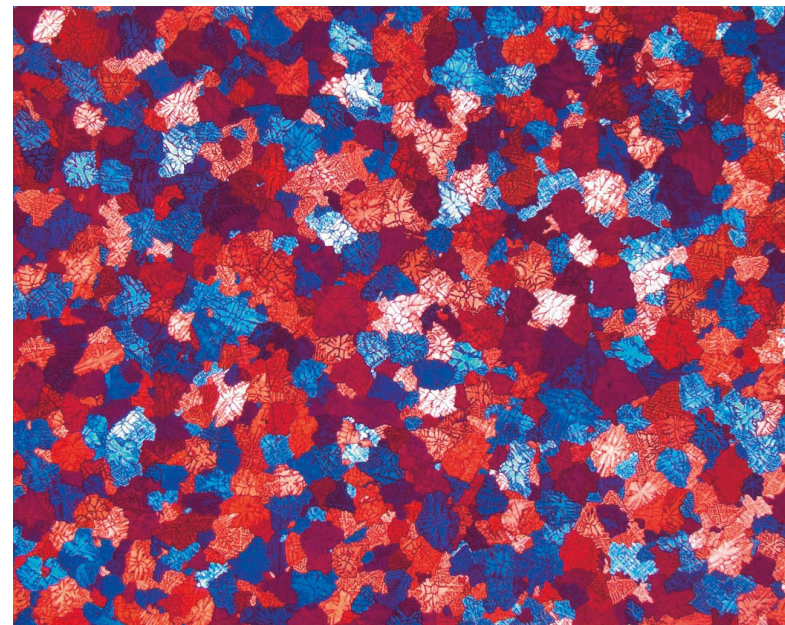
- ▶ **Intermolecular bonding:** involves electrostatic interactions between atoms and/or molecules
- ▶ **Involving charged atoms/molecules:** Charge-charge interactions (*Coulomb forces*) or charge-dipole interactions
- ▶ **Involving polar molecules:** Dipole-dipole, dipole-charge or dipole-induced dipole interactions (*Van der Waals forces*)
 - ▶ Polar molecules: distribution of charges within the molecule
 - ▶ Dipoles may be inherent to the structure of a molecule, or may be induced by the surrounding environment
- ▶ Depending on the type of interactions involved, **different strengths and ranges** will be observed...

The key-role of defects

- ▶ Solids are the result of a fabrication process - **they can't be perfect!**
- ▶ Several types of defects can be found in crystalline materials:
 - ▶ Point defects (0D): vacancies or impurities (solid solutions)
 - ▶ Line defects (1D): dislocations
 - ▶ Planar defects (2D): grain boundaries
 - ▶ Bulk defects (3D): voids or precipitates
- ▶ All these defects may affect the properties of the solid, especially hardness (while elastic modulus is controlled by interatomic or intermolecular forces)

The key-role of microstructure

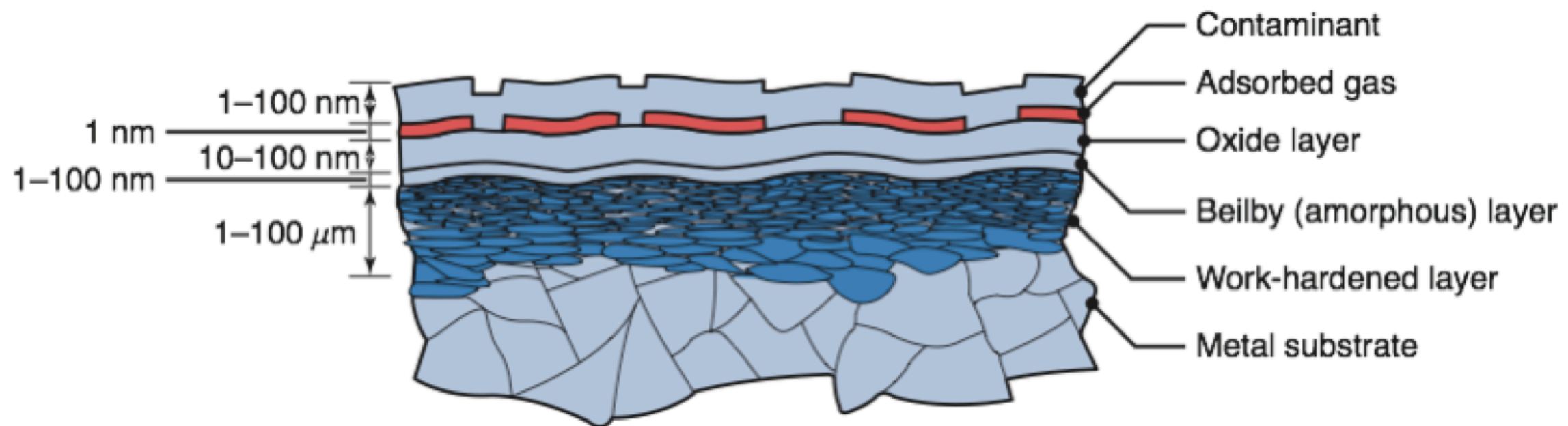
- ▶ Many engineering materials are alloys
- ▶ They consist in an assembly of grains, with different orientations, that might be of different phases
- ▶ The nature, size and distribution of these phases control the mechanical behaviour of the material: hardness, toughness...



- ▶ Study of microstructure:
 - ▶ Diffraction (XRD) for cristallography
 - ▶ Microscopy on cross-section (optical or electron: SEM), EBSD
 - ▶ X-Ray or TEM tomography

Describing a solid surface

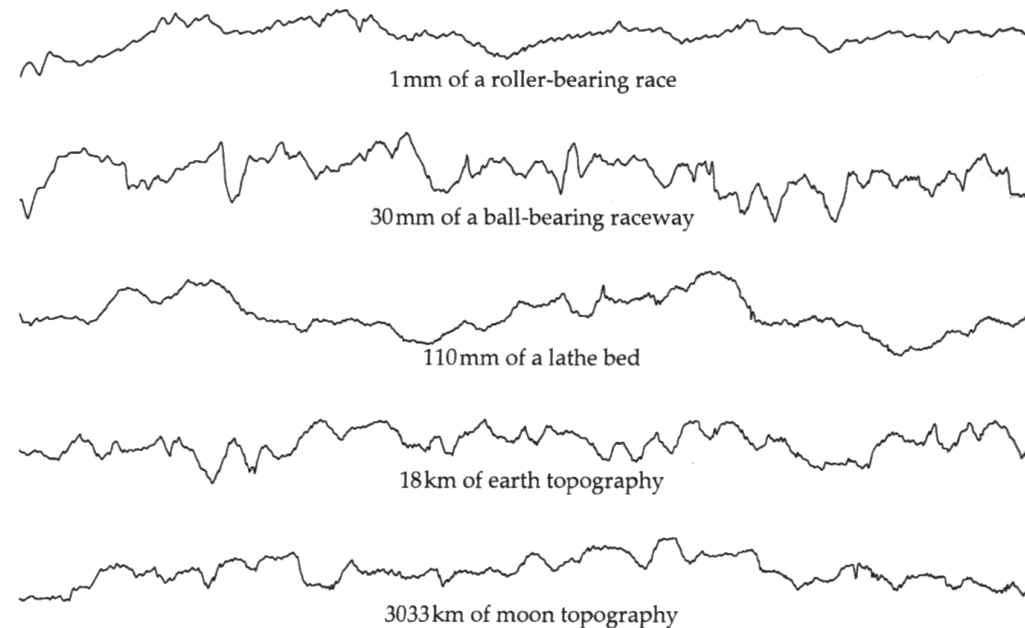
- ▶ Machining process or fabrication process lead to gradients in the microstructure: e.g. change in grain size close to the surface...
- ▶ Since the surface is an interface with the environment, chemical reactions may occur at the surface: oxide layers, adventitious carbon...



- ▶ Even for monocrystalline solids, the edges of a periodic lattice are not favorable: promote “surface reconstruction”
→ always some roughness!

Investigating surface topography

- ▶ Surfaces always exhibit some roughness...
- ▶ Critical role of the considered scale:



- ▶ The probe size is thus critical – Many techniques available!
 - ▶ Tactile profilometry: from simple stylus to Atomic Force Microscopy (AFM)
 - ▶ Laser beam profilometry
 - ▶ Optical methods: interferometric microscopy, confocal microscopy...
- ▶ Don't forget to look at surface morphology!
(e.g. optical or electron microscopy)

Investigating surface topography

▶ Parameters describing the surface:

▶ Height characteristics

▶ Arithmetical mean height

$$R_a = \frac{1}{L} \int_0^L |z| \, dx$$

▶ Root mean square roughness

$$R_q = \sqrt{\frac{1}{L} \int_0^L z^2 \, dx}$$

▶ Maximum peak to valley, skewness (asymmetry), kurtosis...

▶ Spatial characteristics

▶ Autocorrelation function, Power spectral density function...

▶ Multiscale characterisation

▶ Fourier transformation, wavelet transformation...

Investigating surface chemistry

- ▶ Knowing the composition and/or chemistry of a surface is critical for understanding its properties
- ▶ Many surface characterisation techniques are available:
 - ▶ SEM coupled with EDX (Energy Dispersive X-ray spectroscopy)
 - ▶ Vibrational spectroscopies: Raman, FTIR...
 - ▶ Glow Discharge Optical Emission Spectroscopy (GDOES)
 - ▶ Secondary Ion Mass Spectroscopy (SIMS), static (ToF-SIMS) or dynamic
 - ▶ X-Ray Photoelectron Spectroscopy (XPS), Auger Electron Spectroscopy (AES)
 - ▶ Electron Energy Loss Spectroscopy (EELS) in transmission or reflection

Surface energy

- ▶ Surface energy corresponds to the **disruption of interatomic or intermolecular bonds** due to the surface creation
- ▶ Equivalence between surface energy (J/m^2) and surface tension (N/m):
Increasing the size of a surface corresponds to the work of a force

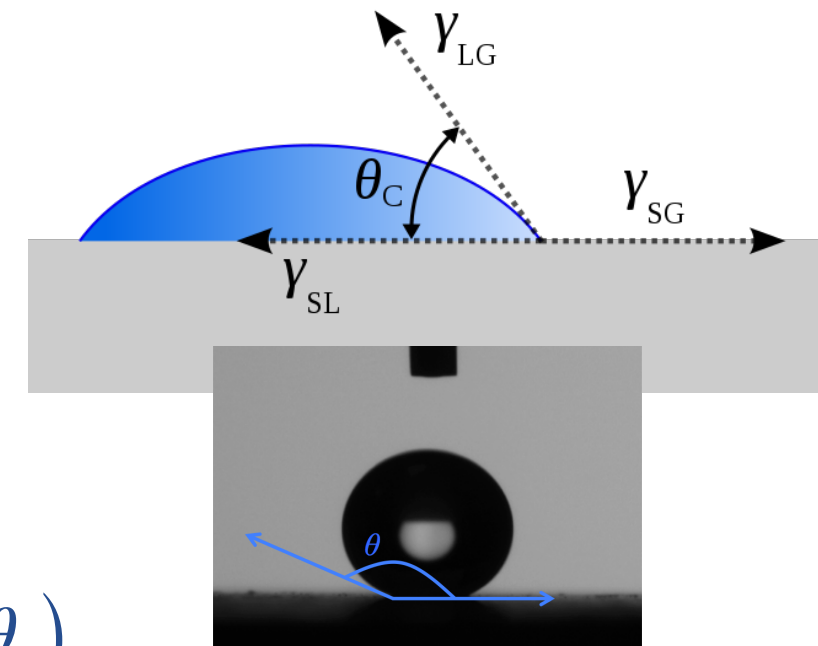
▶ Measuring surface energy:

▶ Contact angle measurements

- ▶ Liquid droplet on a surface

- ▶ Young's equation: $\cos \theta_c = \frac{\gamma_{SG} - \gamma_{SL}}{\gamma_{LG}}$

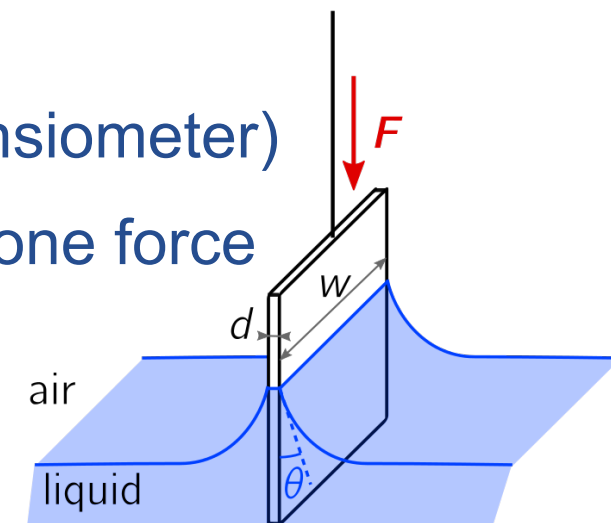
- ▶ Work of adhesion: $W_{adh} = \gamma_{LG} (1 + \cos \theta_c)$



▶ Surface tension measurements (Wilhelmy plate tensiometer)

- ▶ Immersion of a plate with measurement of undergone force

- ▶ $\gamma = \frac{F}{l \cos \theta}$, where l is the perimeter



Surfaces & Friction

Influence of surfaces on friction

Part 2

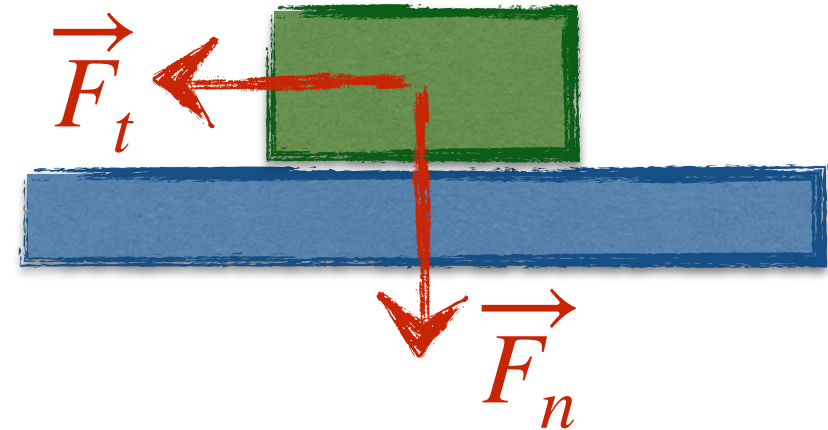
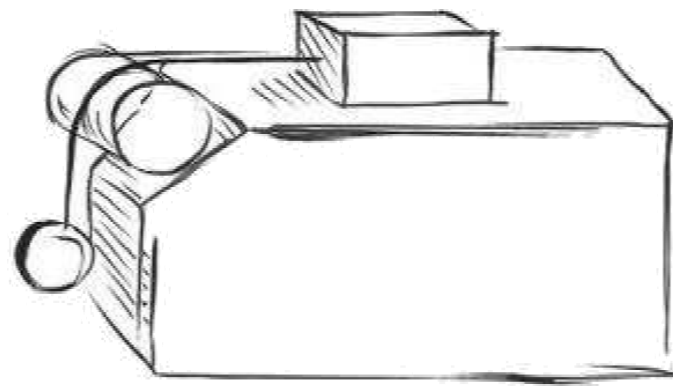
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Defining friction...

Friction: the force resisting to relative motion between solids

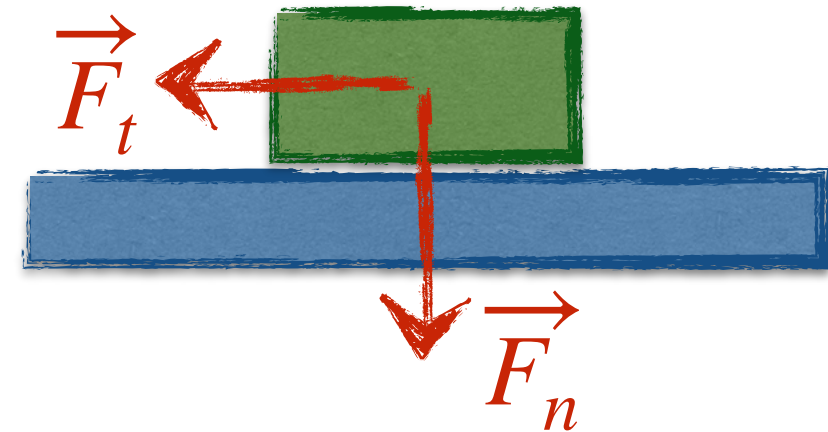
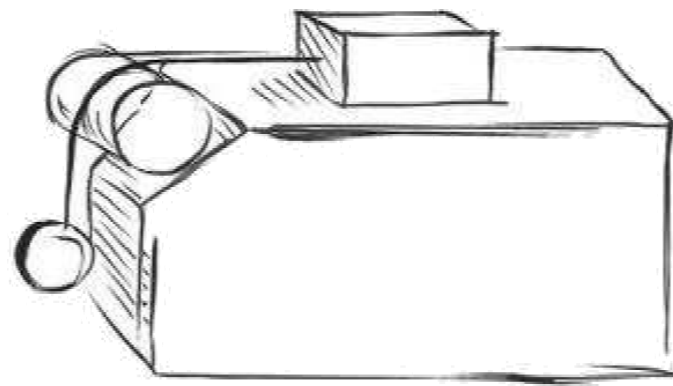


- ▶ **Early laws of dry friction** - Da Vinci, Amontons, Coulomb
 - ▶ *Friction force is proportional to load*
 - ▶ *Friction force is independent of contact area*
 - ▶ *Friction force is independent of sliding velocity*
- ▶ Definition of the **coefficient of friction** μ
Ratio of the tangential force to the normal force:

$$\mu = \frac{F_t}{F_n}$$

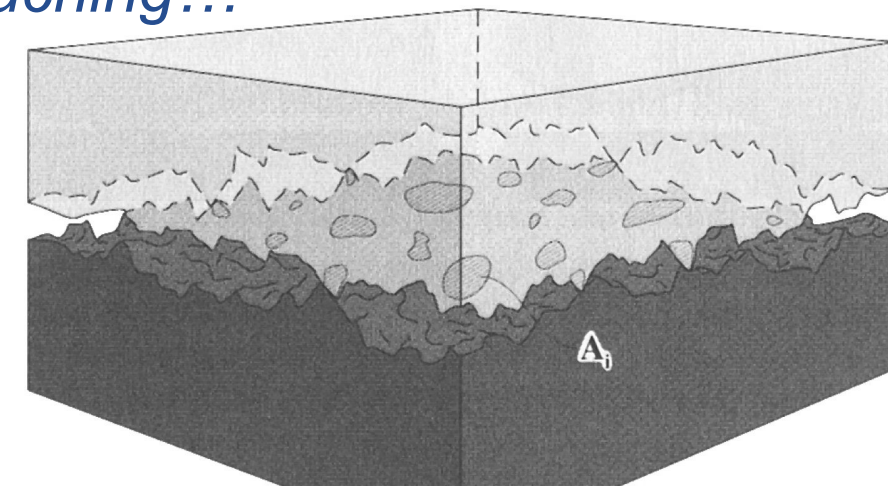
Defining friction...

Friction: the force resisting to relative motion between solids



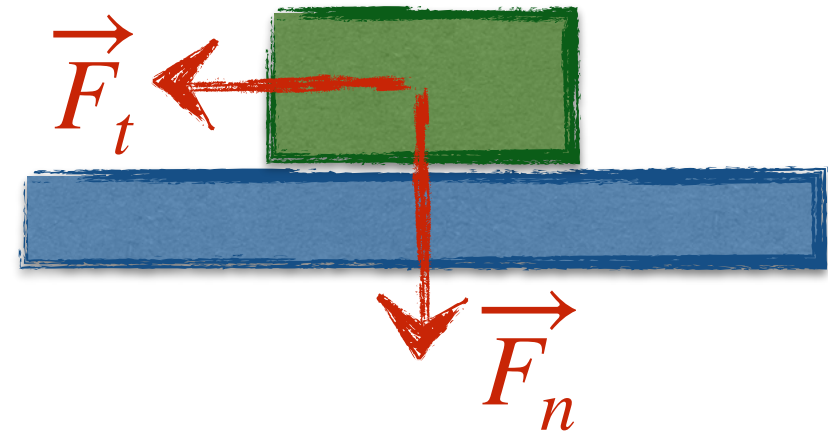
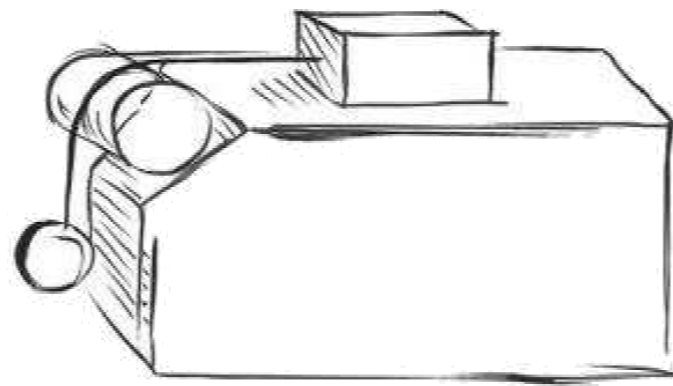
- ▶ **Early laws of dry friction** - Da Vinci, Amontons, Coulomb
 - ▶ *Friction force is proportional to load*
 - ▶ *Friction force is independent of contact area*
 - ▶ *Friction force is independent of sliding velocity*
- ▶ **No effect of apparent contact area!**
Due to roughness, only asperities are touching...
Real vs. apparent contact area

$$A_r \neq A_{app}$$



Defining friction...

Friction: the force resisting to relative motion between solids



- ▶ **Early laws of dry friction** - Da Vinci, Amonton, Coulomb
 - ▶ *Friction force is proportional to load*
 - ▶ *Friction force is independent of contact area*
 - ▶ *Friction force is independent of sliding velocity*
- ▶ No velocity effect proposed, but:
 - Static friction $\geq$ Sliding friction (or “kinetic” or “dynamic”)*
 - Static friction: maximum friction force before sliding occurs*

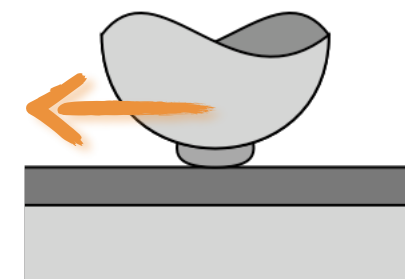
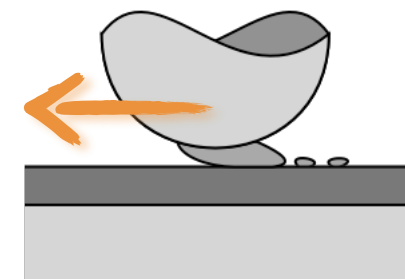
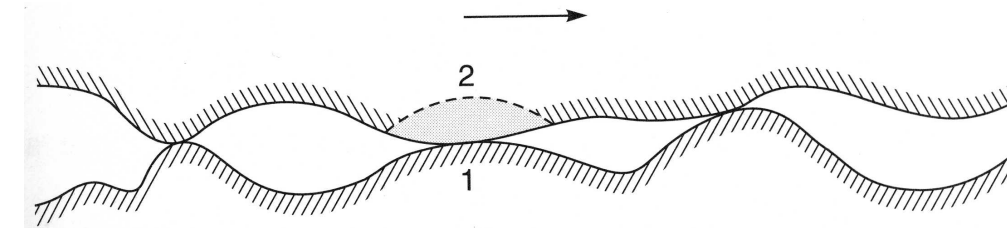
The challenge of lubrication: Velocity accommodation

- ▶ **Lubrication with oils or liquids:** a fluid film separates the solids, allowing an easy shear of the sliding interface
 - ▶ **Hydrodynamic lubrication:** thickness of the fluid film is large compared to the surface roughness
 - ▶ **Elasto-hydrodynamic lubrication** (EHD or EHL): elastic deformation of solid surfaces, creating
 - ▶ **Mixed Lubrication:** some asperity contact, but part of the load is carried by the fluid
 - ▶ **Boundary lubrication:** most of the load is carried by contacting asperities, which are surrounded by the fluid

- ▶ **Solid lubrication:** a material (often a coating) provides an easy shear of the sliding interface

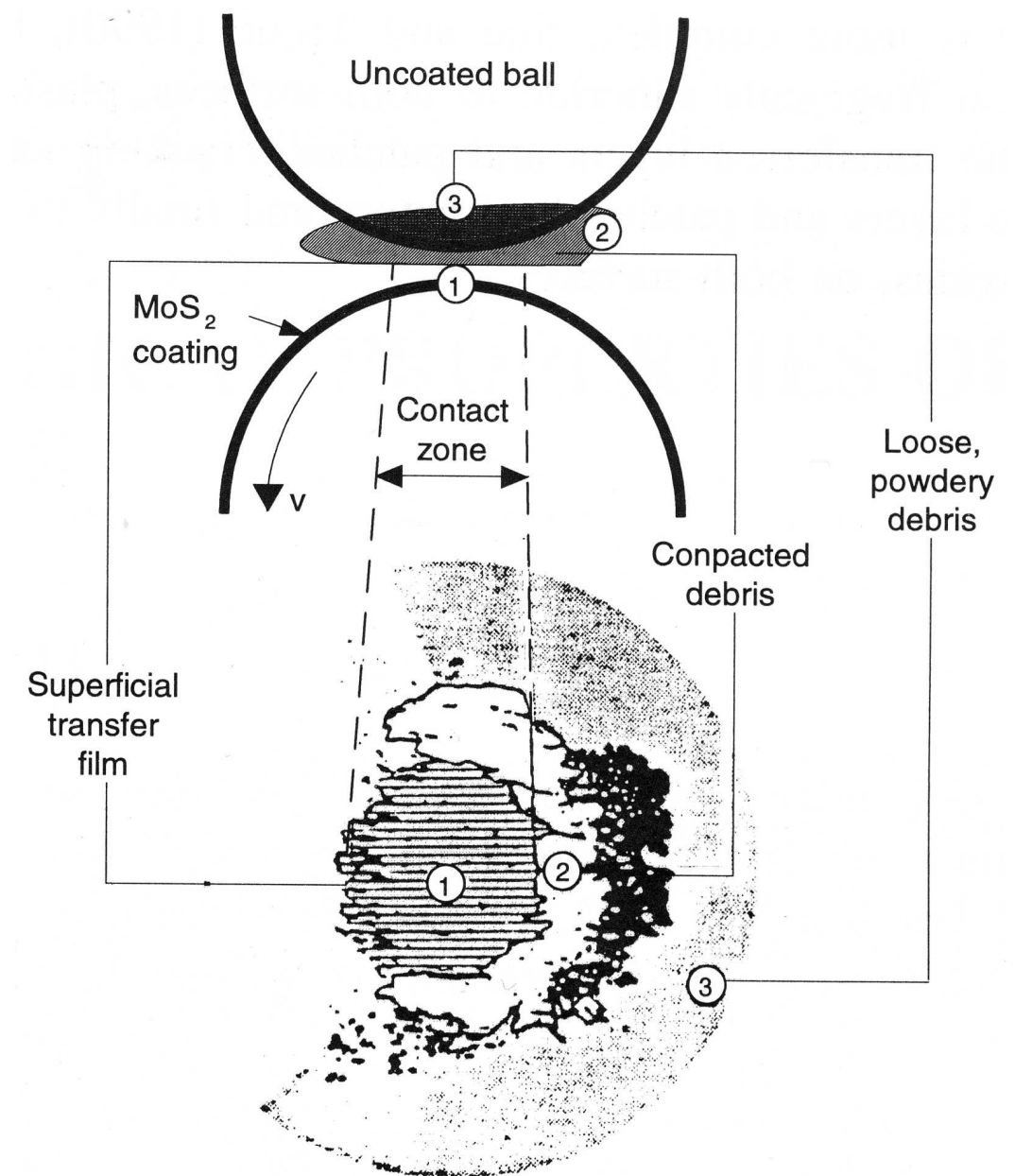
Velocity accommodation in “dry” contacts

- ▶ In “dry” or “solid” contacts, when solid asperities interact, **shear occurs where it’s easier!**
- ▶ In case of seizure, breaking of **adhesive junctions**
 - ▶ at initial interface (1)
 - ▶ inside the weakest material (2) (depending on hardness and brittleness)
- ▶ With solid lubricants, shearing of **interfacial films**:
 - ▶ “Intrafilm flow” or “interfilm sliding”
- ▶ General case: shearing of debris or trapped particles → **third body concept**



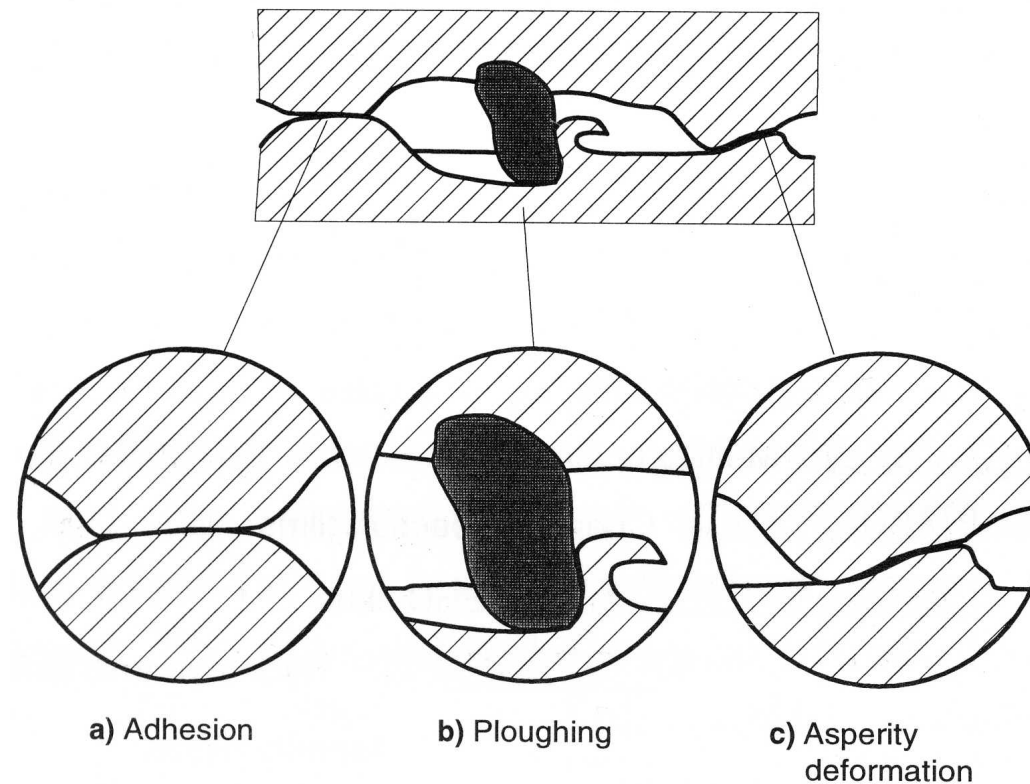
What may be found in a “dry” contact?

- ▶ Flow from one solid to the other
- ▶ Compaction of wear debris
- ▶ Build-up of « tribofilms » or « transfer layer »
- ▶ Chemical reactions between contacting bodies or with the environment



Origins of friction force

- Contributions to the friction force (*Bowden & Tabor*):



- Adhesion: shearing of adhesive junctions

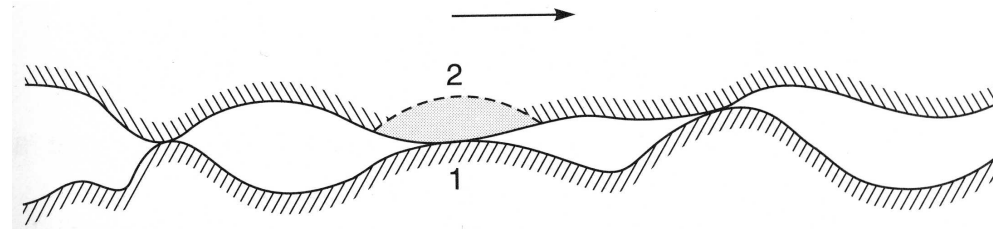
$$F_{adh} = A_r \cdot \tau, \text{ with } A_r: \text{real contact area, } \tau: \text{interfacial shear strength}$$

- Plastic deformations

- Macroscopic: ploughing - abrasion of the softer body
- Microscopic: plastic deformation of contacting asperities

Dry friction of metals: adhesion

- Adhesive phenomena between asperities (*Rabinowicz*)



- Release of adhesive junctions:
 - Controlled by surface energy → strength of interface
 - Controlled by hardness → strength of asperities
- Empirical formula based on experimental results:

$$\mu \simeq 0.3 + C_1 \frac{W_{12}}{H}, \text{ with } W_{12} = C_2 (\gamma_1 + \gamma_2)$$

$$\mu \simeq 0.3 + C_1 C_2 \frac{\gamma_1 + \gamma_2}{H}$$

W_{12} : work of adhesion – γ_1, γ_2 : surface energies
 C_1 : geometrical constant – C_2 : miscibility constant
 H : hardness of softer body

Dry friction of metals: adhesion

- Adhesive phenomena between asperities (*Rabinowicz*)

	W	Mo	Cr	Co	Ni	Fe	Nb	Pt	Zr	Ti	Cu	Au	Ag	Al	Zn	Mg	Cd	Sn	Pb	In
In																				
Pb																				
Sn																				
Cd																				
Mg																				
Zn																				
Al																				
Ag																				
Au																				
Cu																				
Ti																				
Zr																				
Pt																				
Nb																				
Fe																				
Ni																				
Co																				
Cr																				
Mo																				
W																				

$$\mu \simeq 0.3 + C_1 C_2 \frac{\gamma_1 + \gamma_2}{H}$$

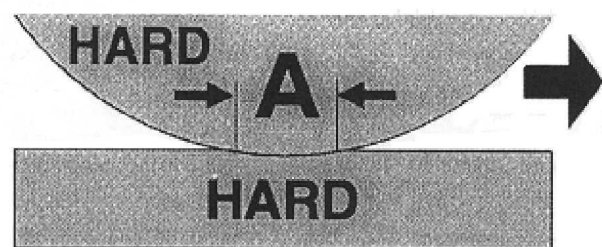
Condition	Symbol	Measured value of C_2
Identical	○	1.00
Compatible	⊙	0.50
Limited compatibility	◐	0.32
Very limited compatibility	◑	0.20
Incompatible	●	0.125

Symbol	Metallurgical solubility	Metallurgical compatibility	Sliding compatibility	Anticipated wear
○	100%	Identical	Very poor	Very high
⊙	Above 1%	Soluble	Poor	High
◐	0.1–1%	Intermediate soluble	Intermediate	Intermediate
◑	Below 0.1%	Intermediate insoluble	Intermediate or good	Intermediate or low
●	Two liquid phases	Insoluble	Very good	Very low

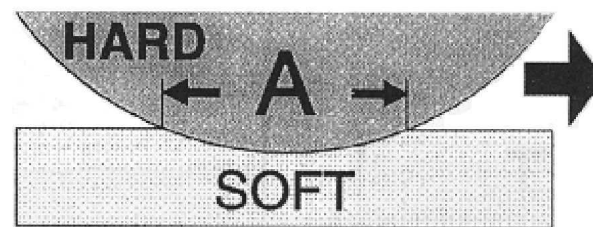
Controlling dry friction: solid lubrication

▶ How to reduce dry friction of metals? (*Bowden & Tabor*)

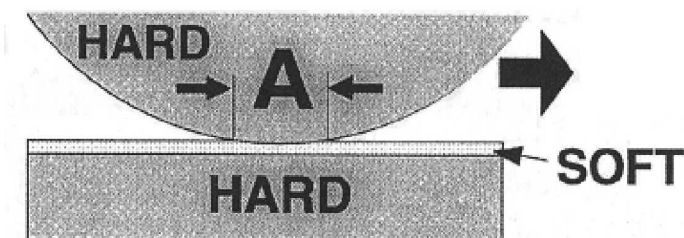
▶ Soft metal film – Playing with A_r & τ in $F_t = A_r \cdot \tau$



τ high
 A_r small



τ small
 A_r high

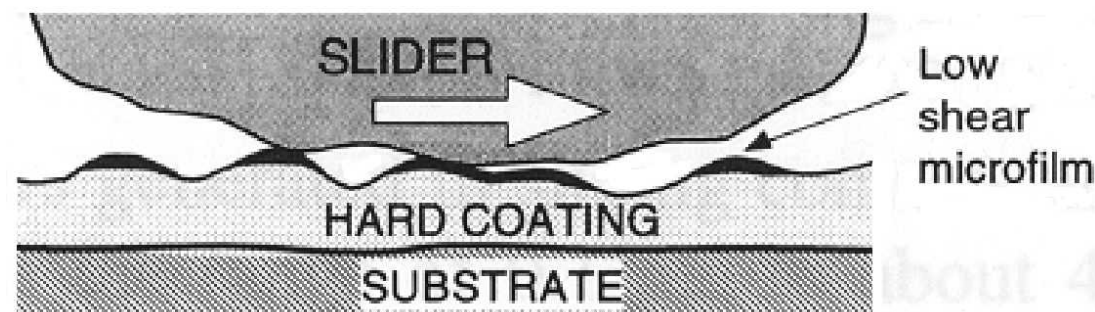


τ small
 A_r small

▶ General case with solid lubricants (*Holmberg & Matthews*)

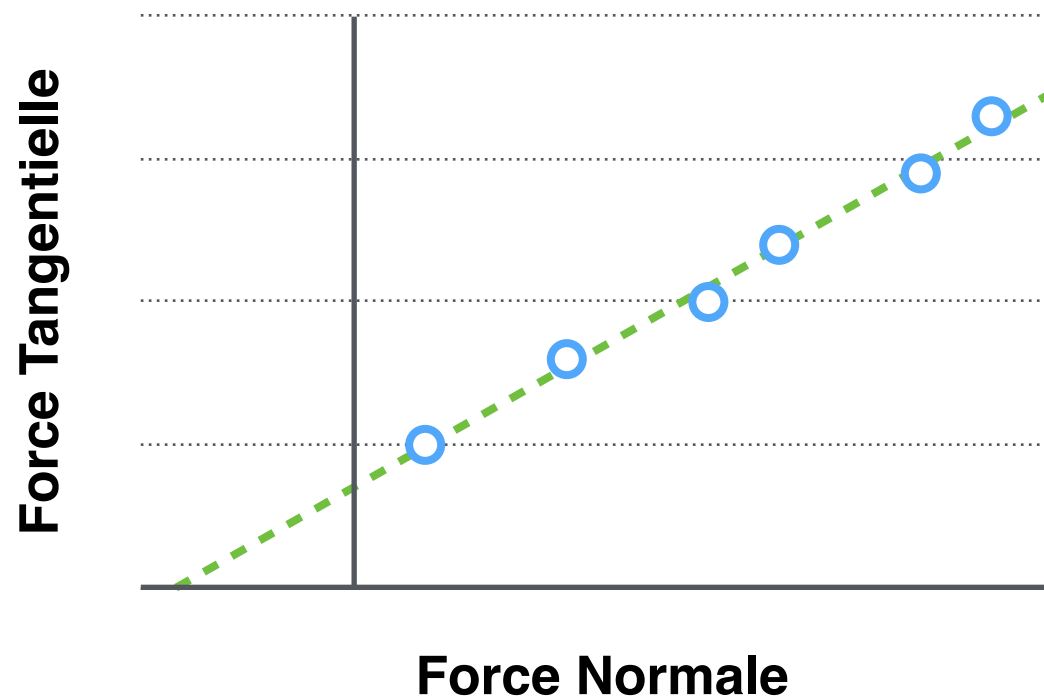
▶ Soft thin coating providing easy shear

▶ Hard and stiff substrates (or underlayers)



The limits of Coulomb's law

- Friction force is not always proportional to load: $\mu \neq \frac{F_t}{F_n}$



- Example: affine behaviour
 - $F_t = \mu \cdot F_n + F_{t_0}$: Threshold in interfacial shear strength?
 - $F_t = \mu \left(F_n + F_{n_0} \right)$: Adhesive forces added to normal force?

The limits of Coulomb's law

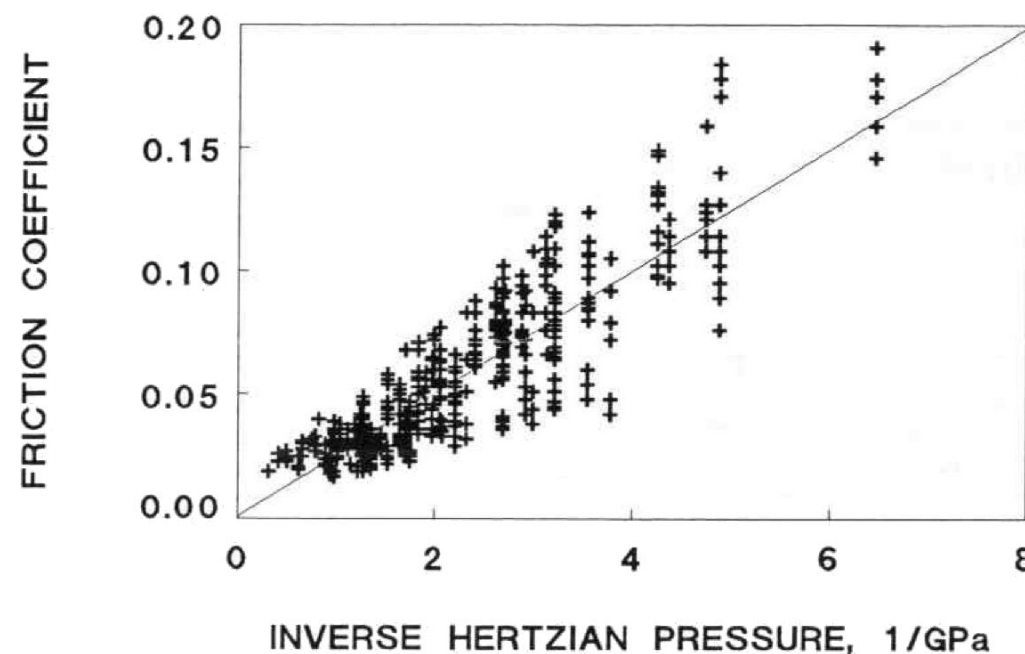
- Both tangential & normal force are proportional to contact area

$$F_t = A_r \cdot \tau \text{ and } F_n = A_r \cdot P$$

$$\mu = \frac{F_t}{F_n} = \frac{\tau}{P}$$

- If μ is changing with normal load, or contact pressure P , then it means that τ depends on contact pressure P

*Example with MoS₂
solid lubricant coatings*



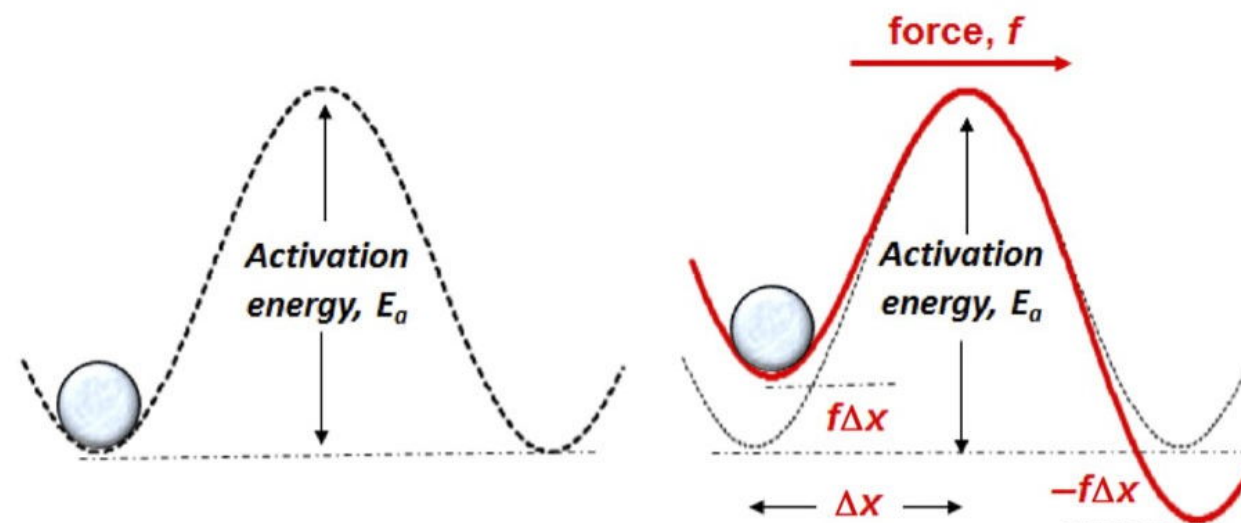
e.g. $\tau = \tau_0 + \alpha P$ implies that $\mu = \frac{\tau_0}{P} + \alpha$ (Singer)

Key role of interfacial material

- ▶ Critical parameters controlling dry friction:
 - ▶ **Shear strength of interface: τ**
Depends on the nature of interfacial material
 - ▶ **Load carrying capacity of the substrates: P**
Elastic deformation as well as roughness affect the contact pressure
- ▶ The nature, composition and properties of the interfacial material are thus critical for understanding friction and its evolution!

Friction-induced chemical changes: Tribocchemistry

- ▶ Producing new compounds through chemical reactions require energy. Several ways to provide the energy:
 - ▶ Photon activation: photochemistry
 - ▶ Electrical activation: electrochemistry
 - ▶ **Thermal activation: thermochemistry**
 - ▶ **Stress-induced activation: mechano-chemistry**

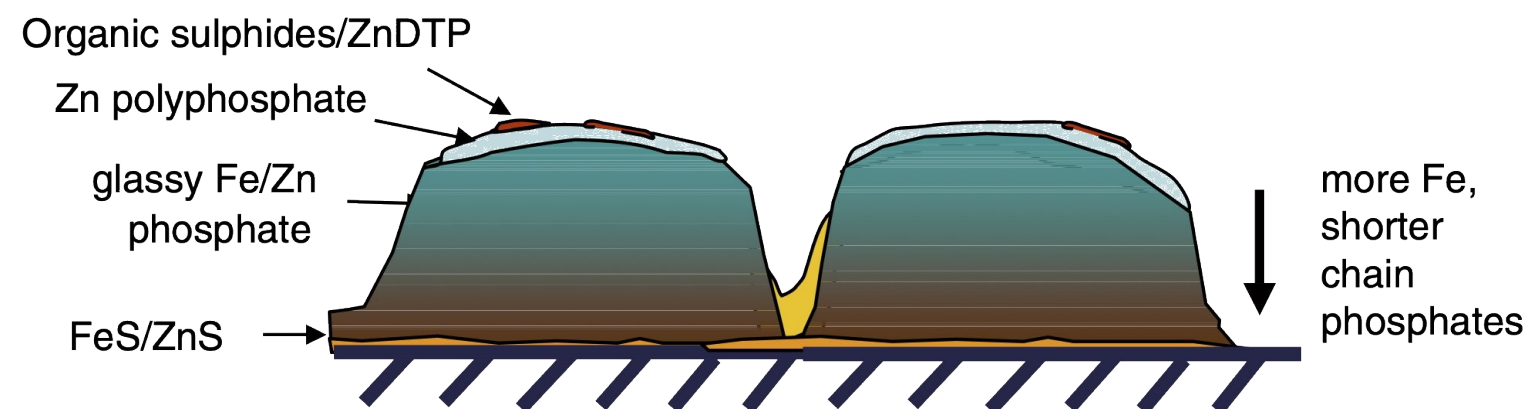
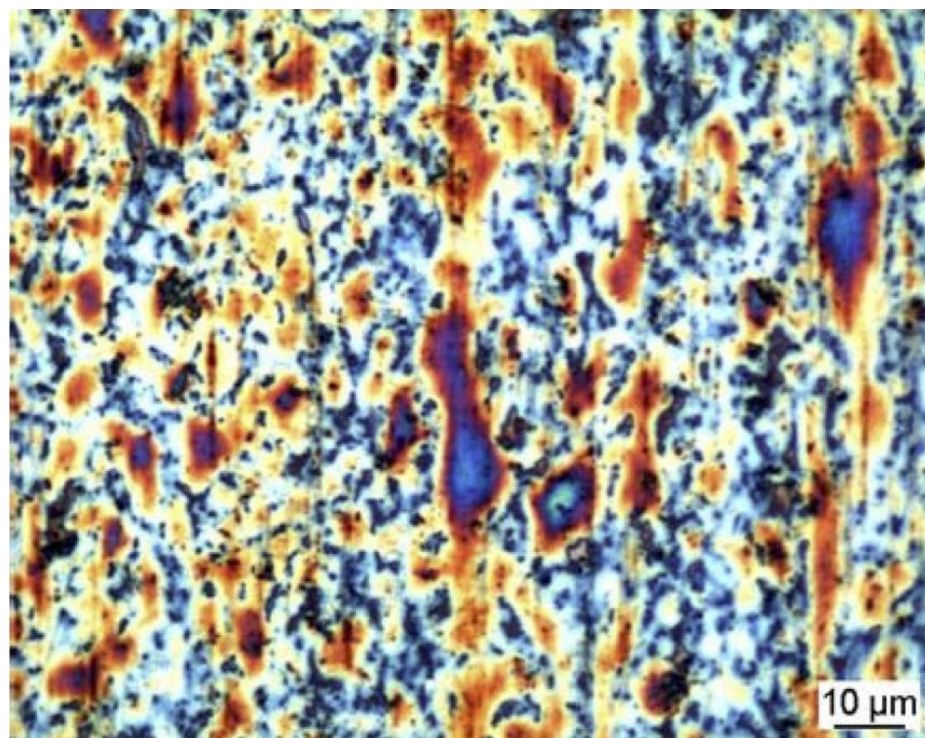


- ▶ *Contacts are « chemical reactors » where reactions may take place between the counterfaces and/or with the environment*

Friction-induced chemical changes: Trib chemistry

- ▶ Trib chemistry: some specificities though!
 - ▶ Reacting species must be “close enough”
 - ▶ Stress distribution in a real contact is highly heterogeneous
 - ▶ Nature of reaction products will affect tribological response

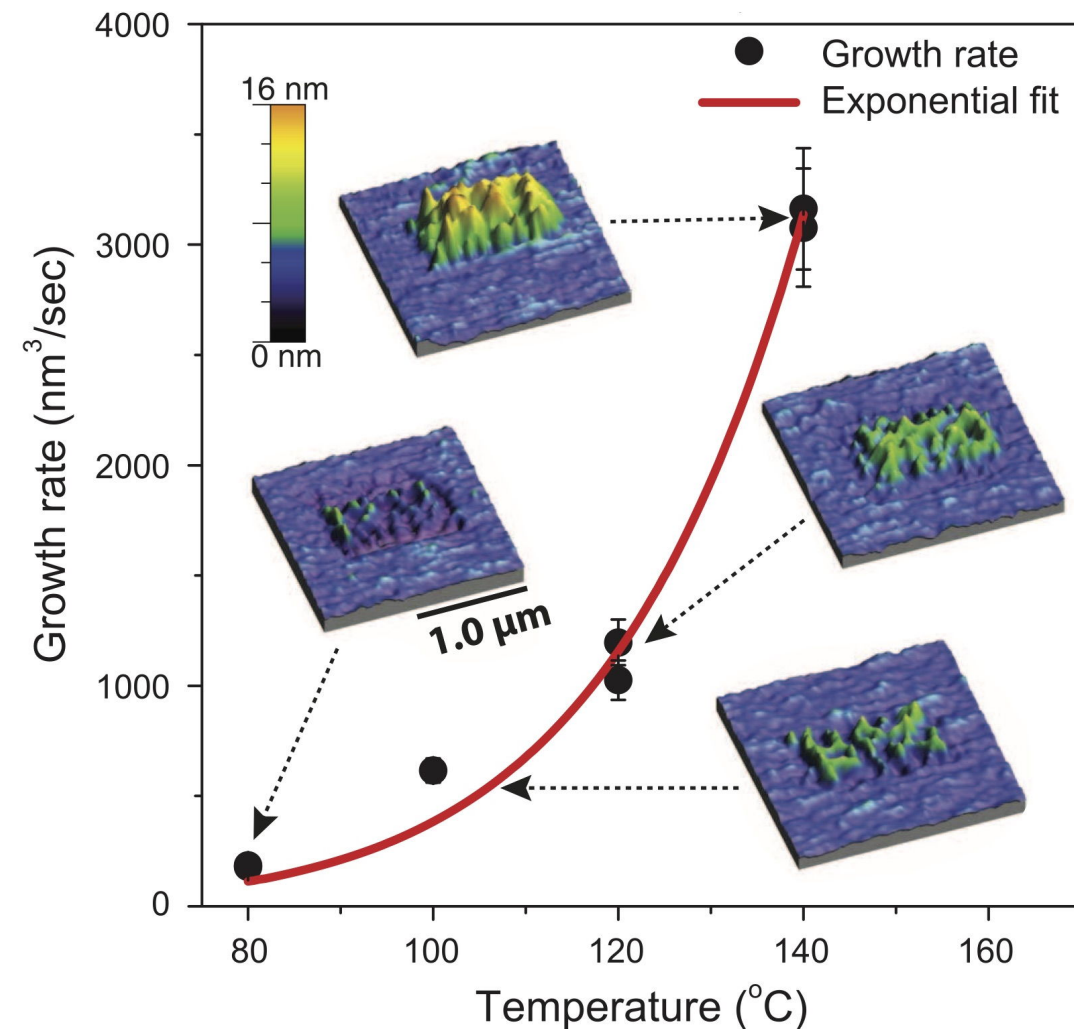
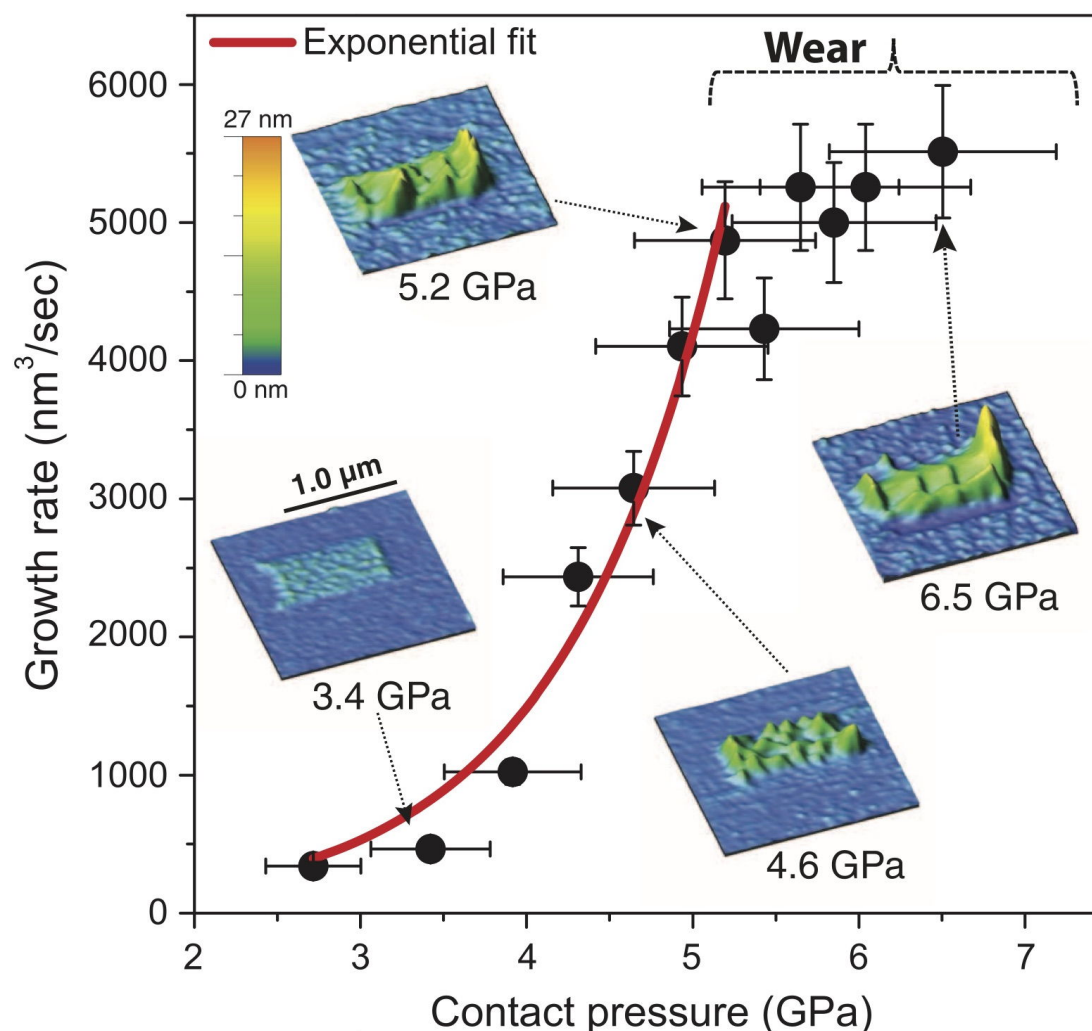
⇒ **Complex structure of the “tribofilms”**
with lateral and vertical gradients



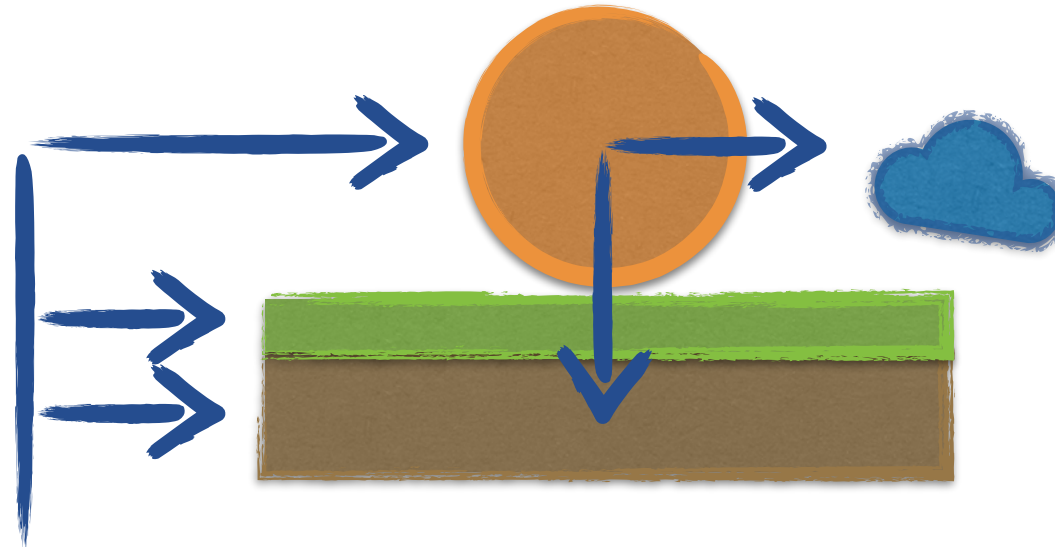
*Example of tribofilm growth on steel from an anti-wear lubricant additive,
Zinc dialkyl-dithiophosphate (ZDDP or ZnDTP)*

Friction-induced chemical changes: Tribocchemistry

- ▶ Competition between stress activation and catalysis
 - ▶ Due to wear, new surfaces are exposed: “nascent surfaces”
 - ▶ Presence of metal or oxides may affect chemical processes
 - ▶ Yet experiments with Atomic Force Microscopy (AFM) clearly evidence a stress and temperature activation



Key tribological parameters



Intrinsic parameters: Materials

- ▶ **Surfaces & interfaces**
 - ▶ Composition & chemistry
 - ▶ Roughness
- ▶ **Coatings**
 - ▶ Composition & chemistry
 - ▶ Structure & thickness
 - ▶ Adhesion to substrate
 - ▶ Mechanical properties
- ▶ **Substrates**
 - ▶ Composition & chemistry
 - ▶ Structure
 - ▶ Mechanical properties

Extrinsic parameters: System

- ▶ **Contact parameters**
 - ▶ Geometry & applied forces
 - ▶ Contact pressure
- ▶ **Kinematic parameters**
 - ▶ Nature of relative motion
 - ▶ Speed, length
 - ▶ Frequency of exposure
- ▶ **Environmental parameters**
 - ▶ Nature & pressure of gases or presence of liquid
 - ▶ Temperature
 - ▶ External solid particles

Adjusting contact severity...

▶ **Geometry**

- ▶ Point contact / Line contact / Surface contact
- ▶ Increasing apparent contact area
- ▶ Decreasing contact pressure

▶ **Applied force**

- ▶ Affects contact area and pressure
- ▶ Contact computations: Hertz, K.L. Johnson...
- ▶ Maximum stress beneath the surface

▶ **Sliding velocity / contact frequency**

- ▶ Contact temperature
- ▶ Kinetics of tribochemical reactions

▶ **Environment**

- ▶ Nature & reactivity of the environment
- ▶ Imposed temperature

Playing with kinematics...

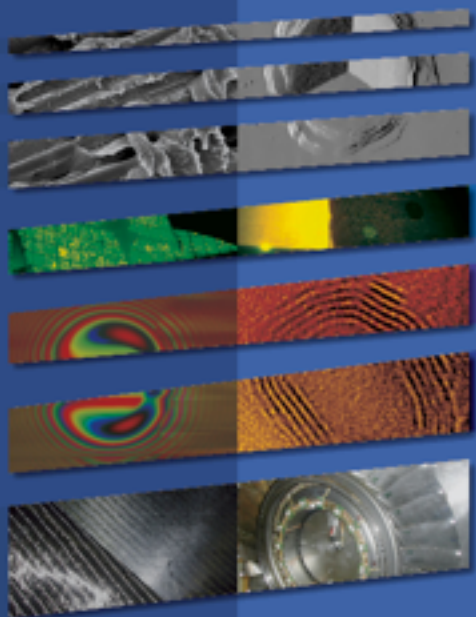
- ▶ Different **type of motion**: linear, rotating / continuous or reciprocating
- ▶ **Dwell time**: time between passes – may affect chemical reactions with environment
- ▶ **Kinematic lengths** of both counterparts: asymmetric nature of most tests!

▶ *Linear ball-on-flat case*

- ▶ Distance traveled by a point on the ball: $L_{ball} = l \cdot N$
- ▶ Distance traveled by a point on the flat: $L_{flat} = 2a \cdot N$
- ▶ With $2a = 100 \mu m$ & $l = 5 mm$, ratio: $\frac{L_{ball}}{L_{flat}} = \frac{l}{2a} \simeq 50$

▶ *Rotating ball-on-disk case*

- ▶ Distance traveled by a point on the ball: $L_{ball} = 2\pi R \cdot N$
- ▶ Distance traveled by a point on the flat: $L_{flat} = 2a \cdot N$
- ▶ With $2a = 100 \mu m$ & $R = 15 mm$, ratio: $\frac{L_{ball}}{L_{flat}} = \frac{2\pi R}{2a} \simeq 1000$



Surfaces & Friction

Solid lubrication processes

of Diamond-Like Carbon

Part 3

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Solid lubrication processes of Diamond-Like Carbon

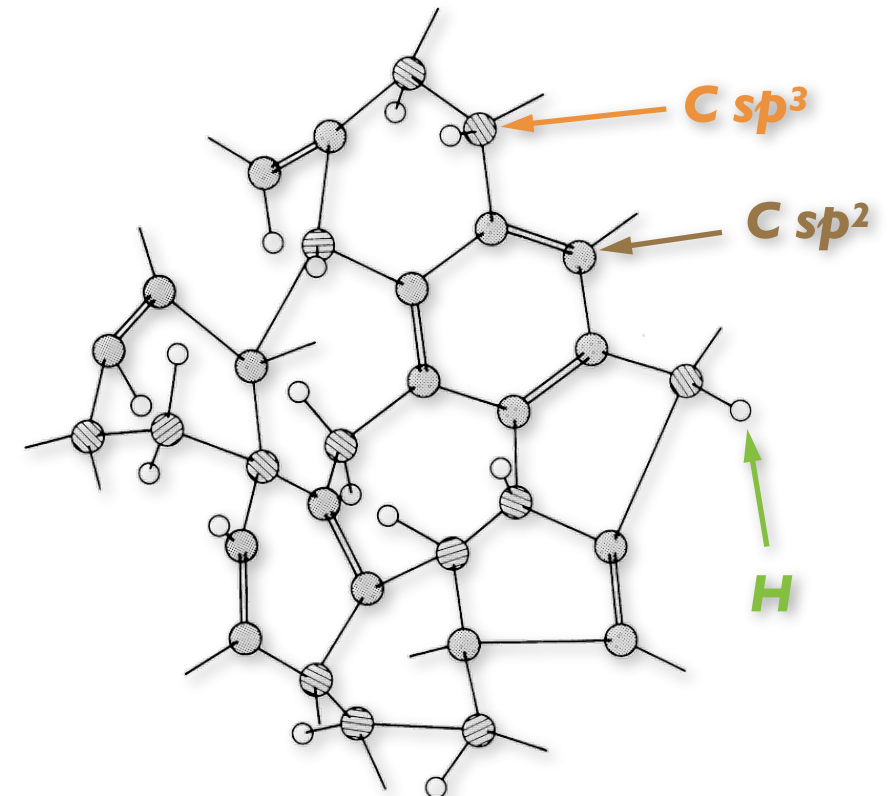
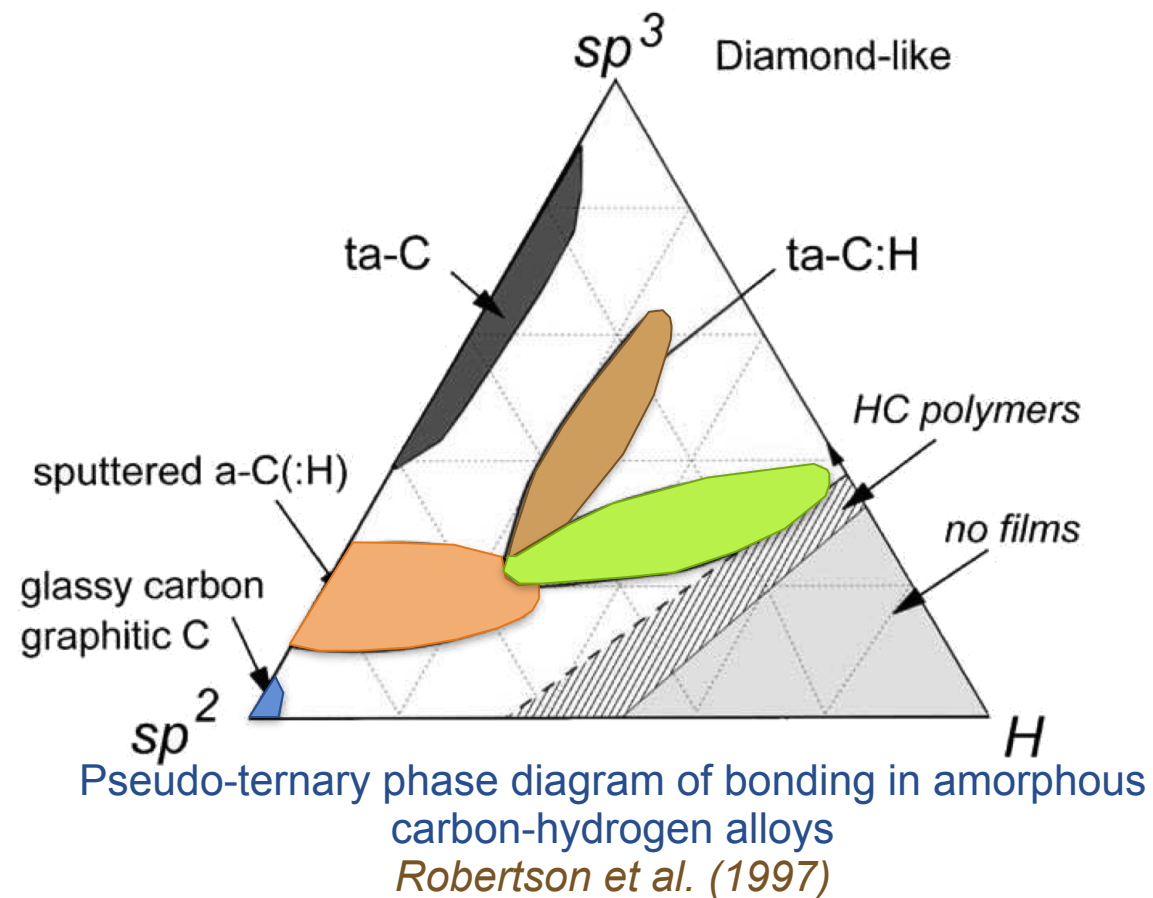
- ▶ **Introduction to DLC coatings**
- ▶ **Role of surface chemistry**
- ▶ **Role of surface topography**
- ▶ **Interactions with environment**
- ▶ **Discussion & summary**

Diamond-Like Carbon: Popular tribological coatings...



- ▶ DLC: a family of hard amorphous carbon films
- ▶ Provide low friction and wear:
good performances as solid lubricants
- ▶ Many industrial applications...

... An amorphous carbon structure...



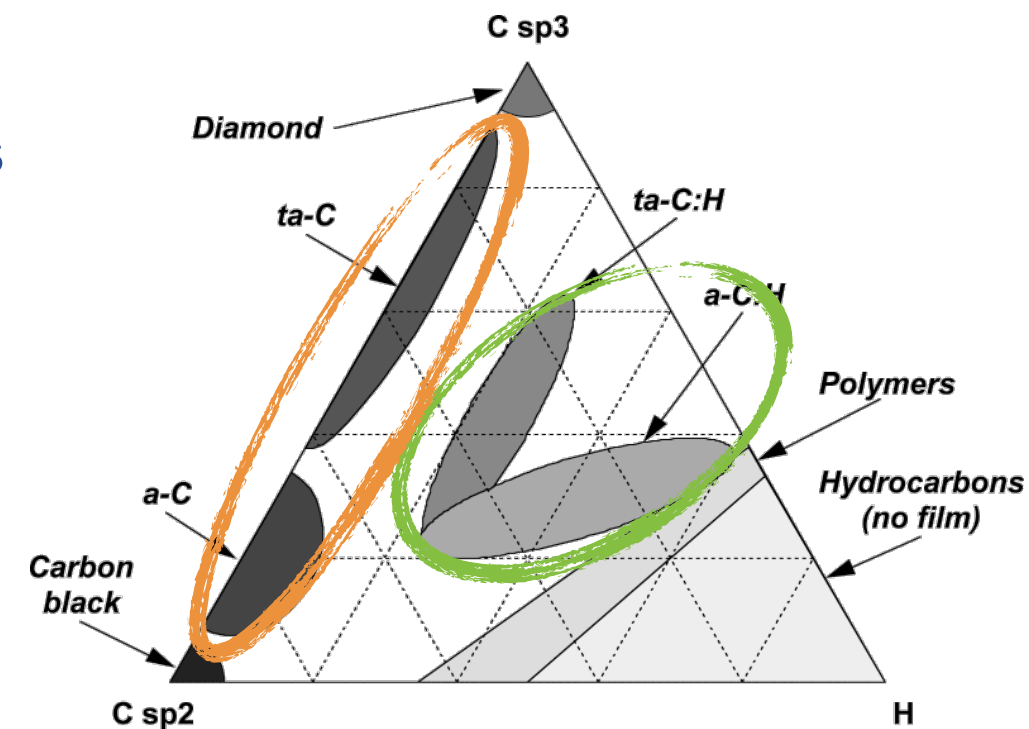
Random covalent network model of hydrogenated amorphous carbon films
Angus et al. (1992)

► Metastable amorphous DLC structure:

- “Random Covalent Network” of sp^2 C, sp^3 C, H
... with defects: dangling bonds, entrapped H_2 or CH_4 ...
- Clustering of sp^2 C: aromatic rings (6-fold C rings)
... with defects: 5- or 7- fold rings (non planar clusters...)
- Graphite is the stable form of carbon,
but high disorder may hinder long-range ordering

... With versatile properties...

- ▶ **Large variety of DLC coatings:**
many different structures & compositions
depending on deposition process ...
⇒ wide range of properties
- ▶ **Physical Vapor Deposition (PVD)**
for hydrogen-free a-C and ta-C
- ▶ **Chemical Vapor Deposition (CVD)**
for hydrogenated a-C:H and ta-C:H

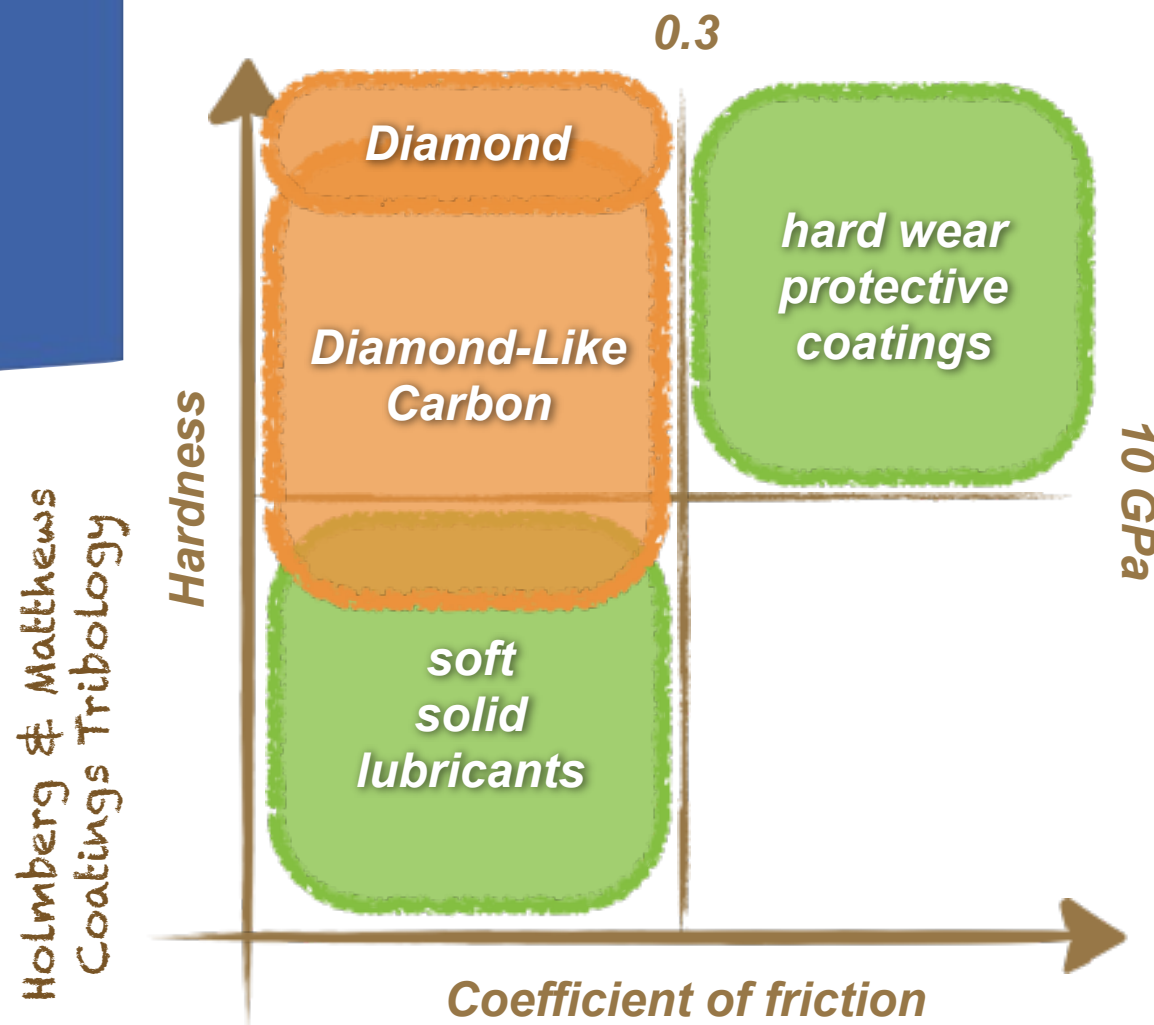


Hydrogen content	< 1 to > 50 at.%
Percentage of sp^3	20 to 90%
Optical gap	0.4 to 4 eV
Compressive stress	up to few GPa
Surface energy	< 20 to > 60 mN.m ⁻¹
Thermal stability	up to ~300°C

	a-C	a-C:H	ta-C	ta-C:H
Hardness (GPa)	10 - 20	2 - 30	25 - 70	25 - 60
Elastic modulus (GPa)	150 - 200	50 - 250	200 - 650	150 - 300
H/E ratio	0.08 - 0.1	0.1 - 0.16	0.1 - 0.2	0.16 - 0.2

- ▶ As hard or harder than steel or most metallic substrates
- ▶ Comparable or lower elastic modulus (except high sp^3 content ta-C)
- ▶ Higher H/E ratio (~ strain to failure)

... But a tribological paradox!



Archard's law

The harder the more wear-resistant
Nitrides, carbides, ceramic coatings

$$V_{\text{worn}} = \frac{k}{H} \cdot F_n \cdot L$$

Bowden & Tabor

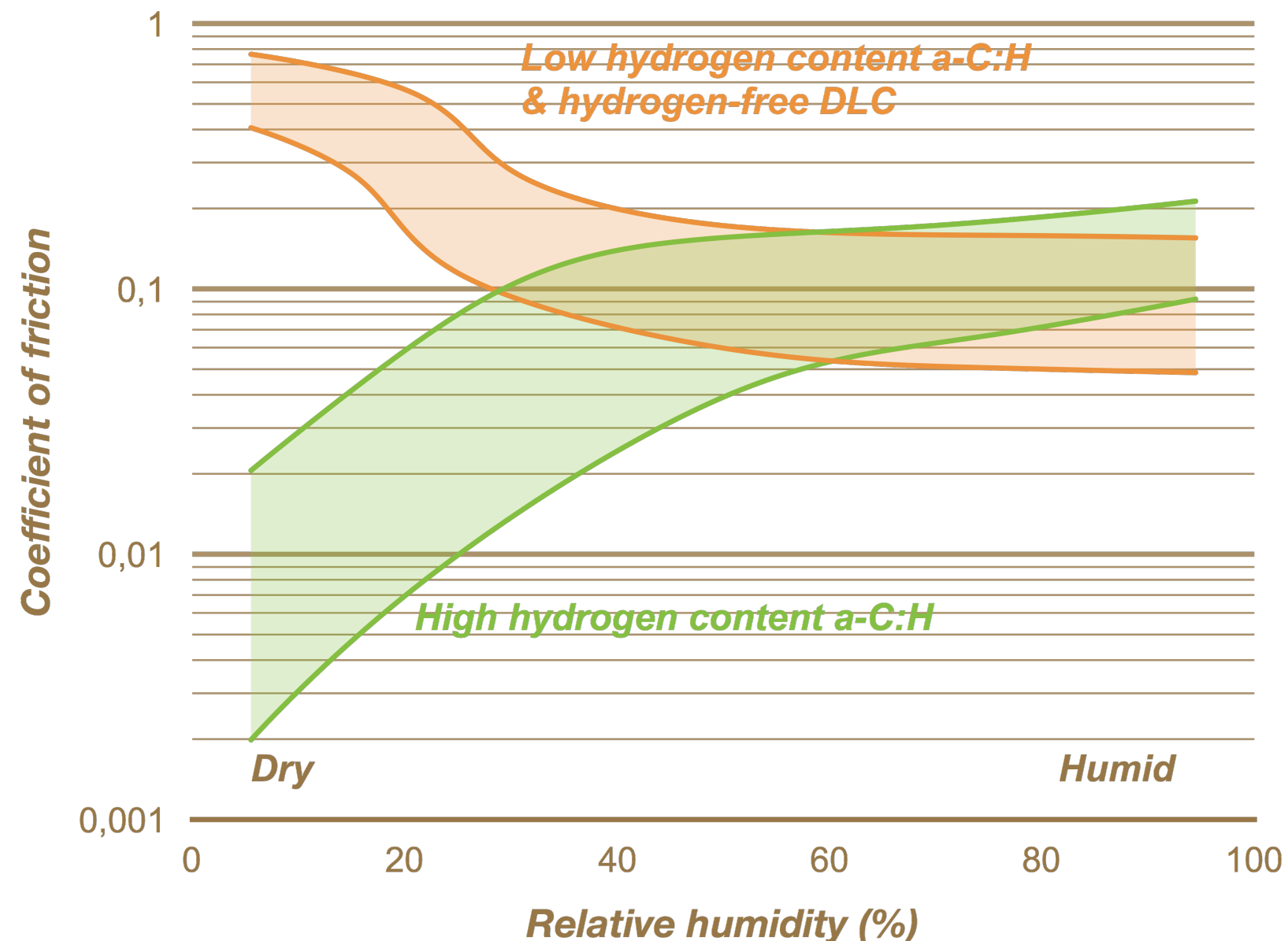
Easy shear thin film trapped
between hard and stiff substrates
Soft metals, lamellar solids...

$$F_t = A_r \cdot \tau$$

How can DLC be both hard and easy to shear?

... Yet some limitations!

- ▶ Strong sensitivity to environment and coating composition!
- ▶ Versatility of the tribological performance...
...dependence on deposition process parameters



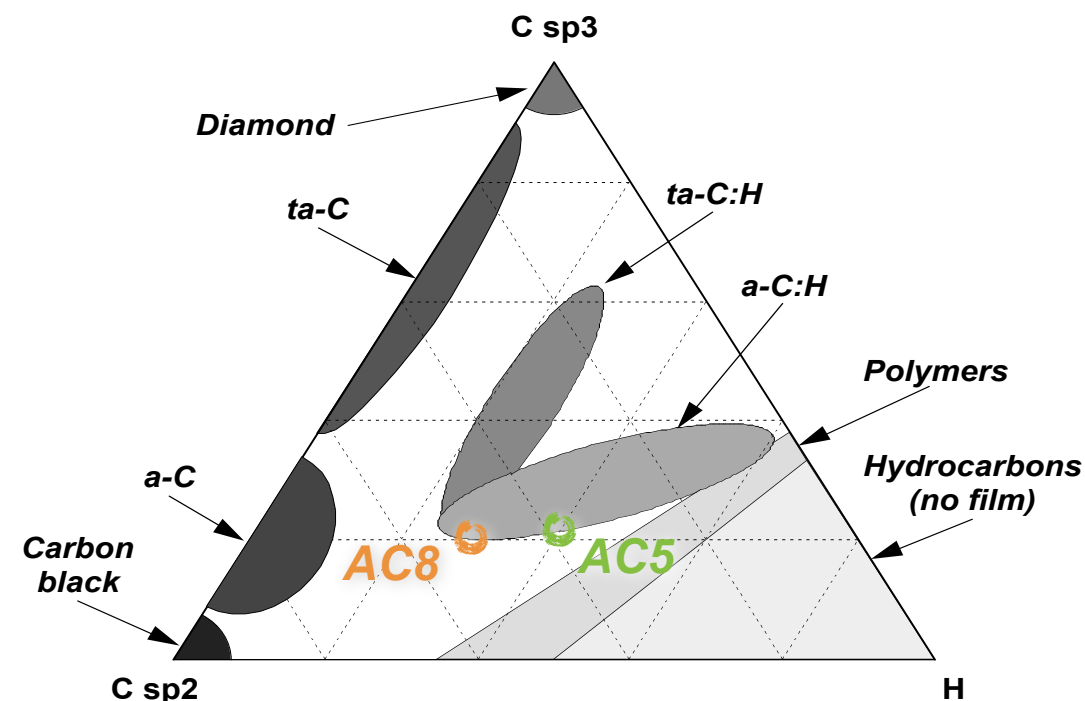
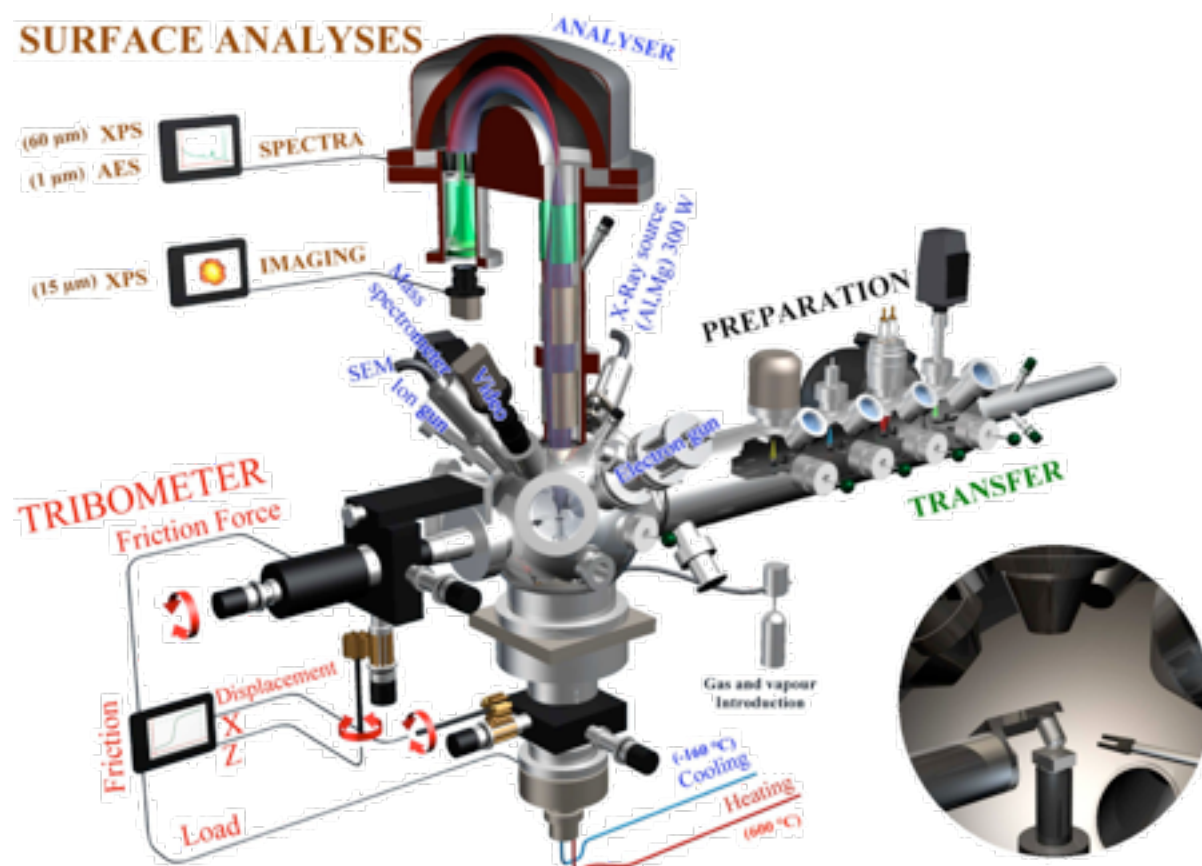
Solid lubrication processes of Diamond-Like Carbon

- ▶ Introduction to DLC coatings
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Tribological experiments on “model” DLC

Analytical UHV tribometer

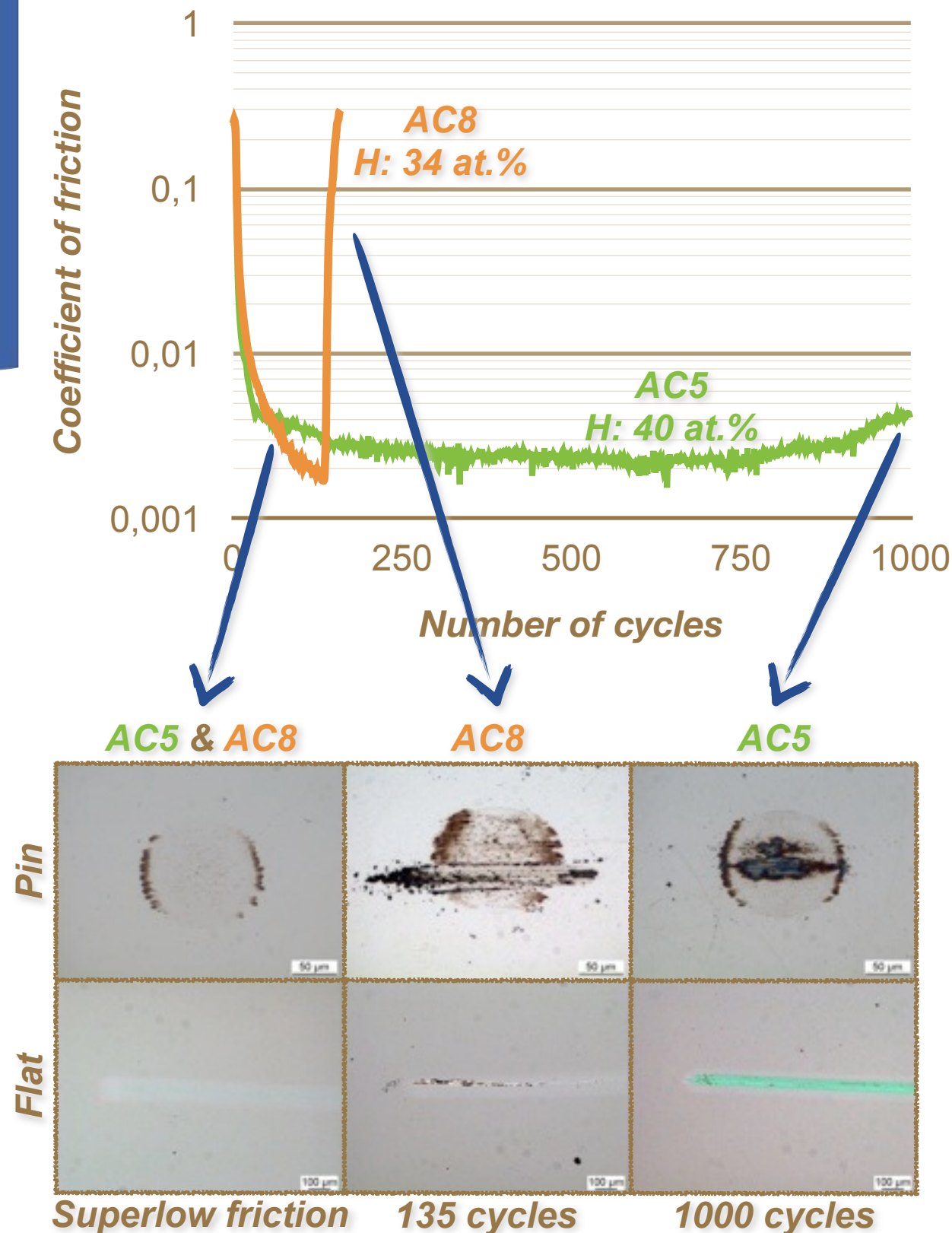
Linear reciprocating motion
DLC (1 μm) on Si(100)
Environment: UHV ($<10^{-6}$ Pa) or pure gases
Sliding speed: 0.5 mm/s
Pin material: 52100 bearing steel
Pin radius: 8 mm
Normal force: 3-5 N
Max. Hertz pressure: ~ 550 MPa
Contact width ~ 100 μm
Macroscopic contact



	dc-PECVD	AC8	AC5
Precursor		C_2H_2	C_2H_2
Flow rate		10 sccm	10 sccm
Pressure		100 mTorr	200 mTorr
Bias voltage		-800 V	-500 V
Carbon content		66 at.%	60 at.%
C sp ³		30%	35%
C sp ²		70%	65%
Hydrogen content		34 at.%	40 at.%
Free H (FTIR)		43%	27%
Free H (NMR)		7%	2%
Hardness		10.5 GPa	7.5 GPa
Elastic modulus		80 GPa	62 GPa

Donnet & Grill, Surf. Coat. Technol. 1997
Donnet et al., J. Appl. Phys. 1999
Bec et al., Phil. Mag. 2006

Friction of a-C:H in UHV



Comparison of these 2 a-C:H films

AC8: 34 at.% of H – **AC5:** 40 at.% of H

Superlow friction is achieved
($\mu < 0.01$)

For **AC8**, drastic friction increase occurs after few tens of cycles
($> \times 100$)

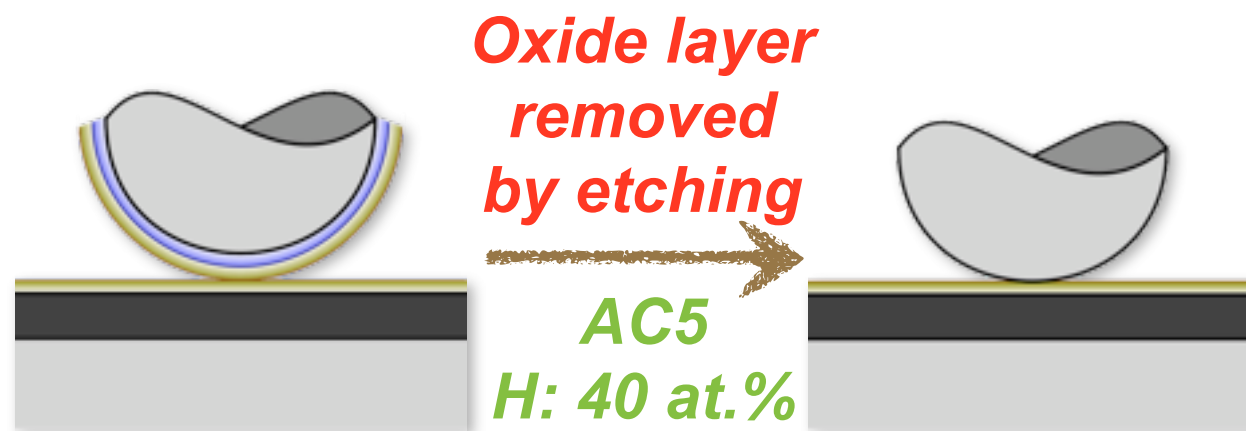
For **AC5**, small friction increase occurs after few hundreds of cycles
($< \times 10$)

Tribofilm is formed during running-in

Drastic friction increase correlated with **removal of tribofilm**

Key-role of hydrogen content?

Surface chemistry & tribofilm build-up

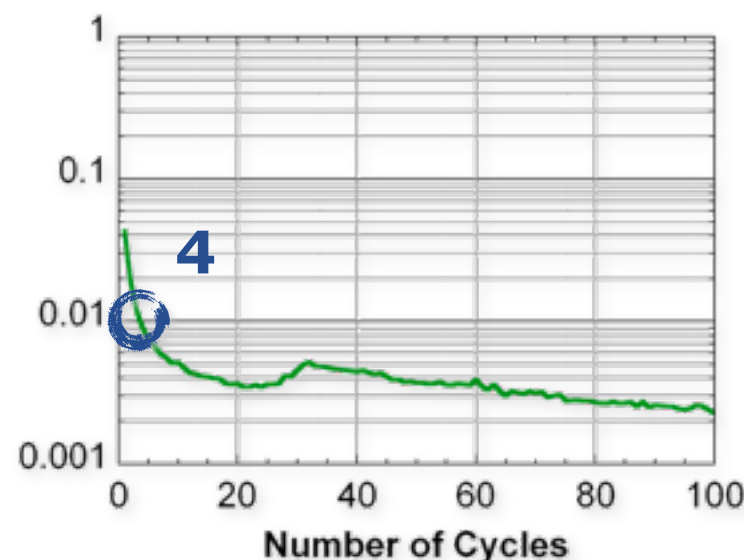
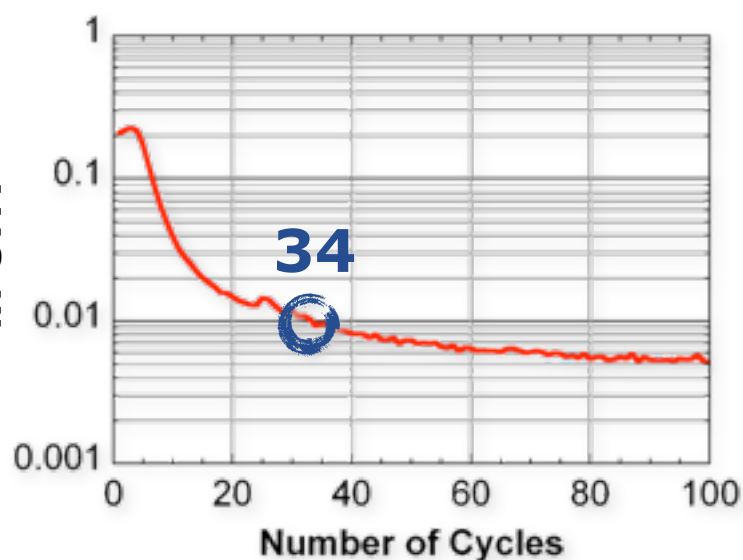


"Tribofilm"

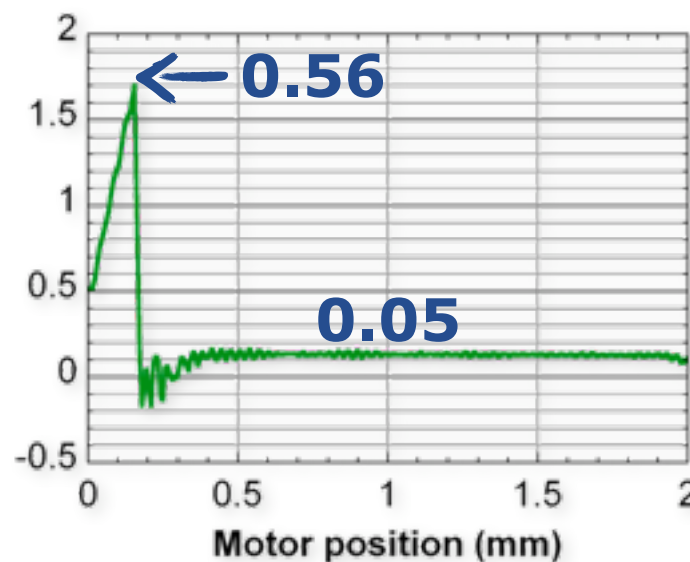
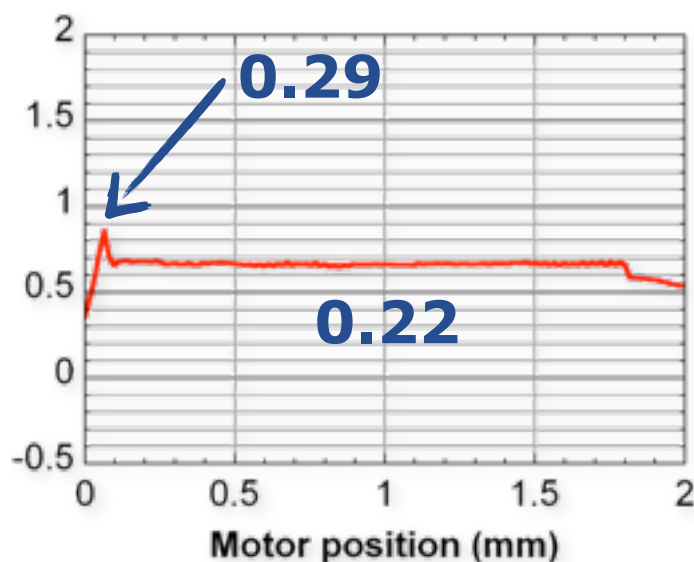
Interfacial material on counterface could be different from initial a-C:H

≠ "Transfer film"

Coefficient of friction in UHV



Friction force during first cycle (N)



Removal of iron oxide

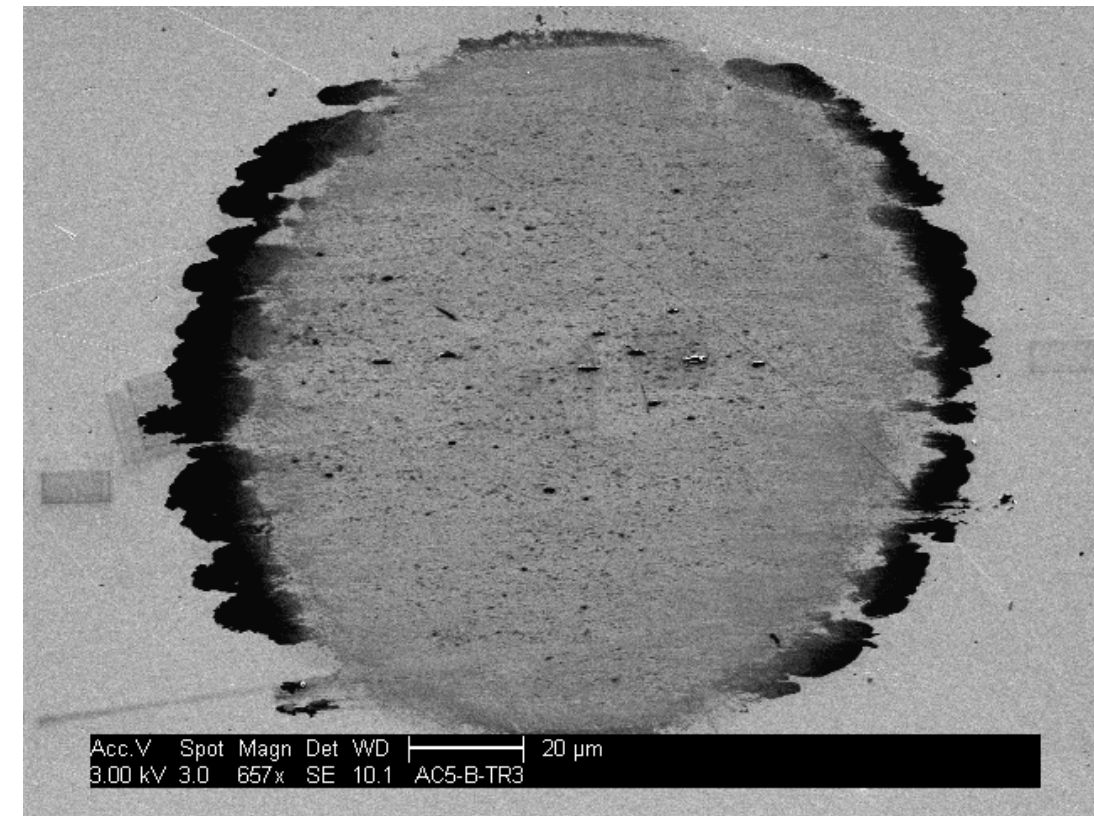
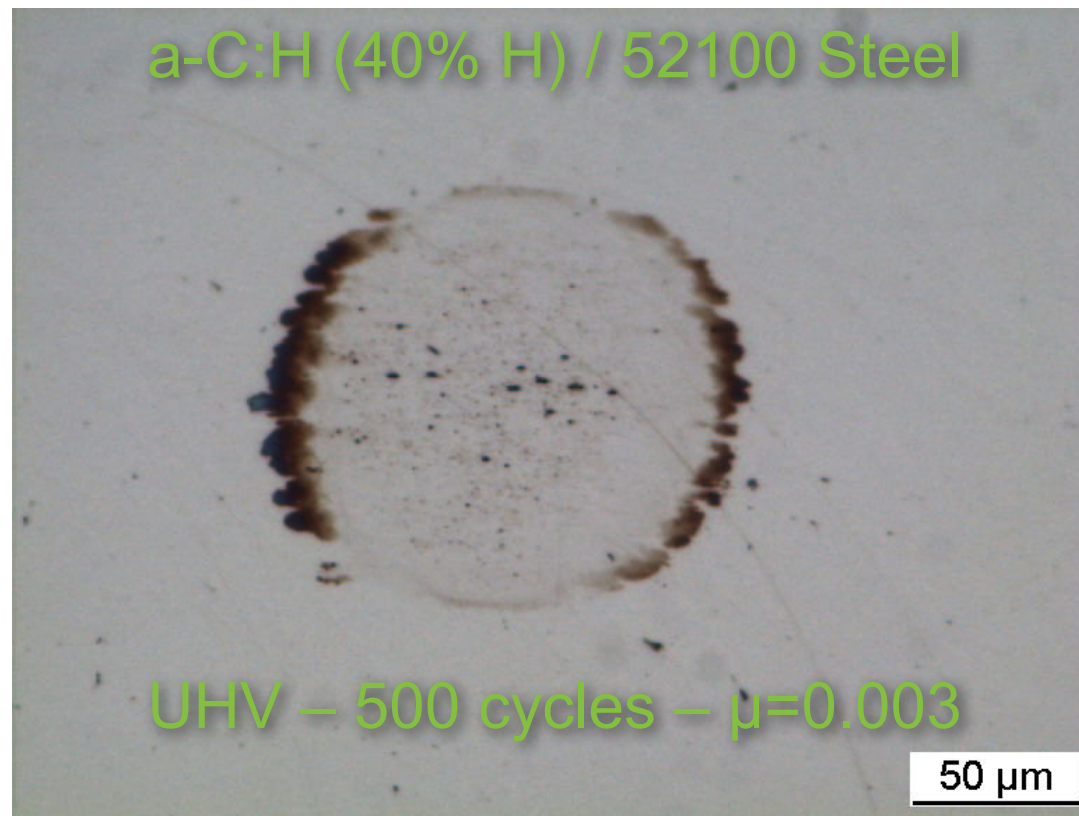
Strong adhesion

Faster tribofilm build-up

Faster friction decrease

Key role of tribofilm build-up

- ▶ Tribofilm grown on metallic counterface

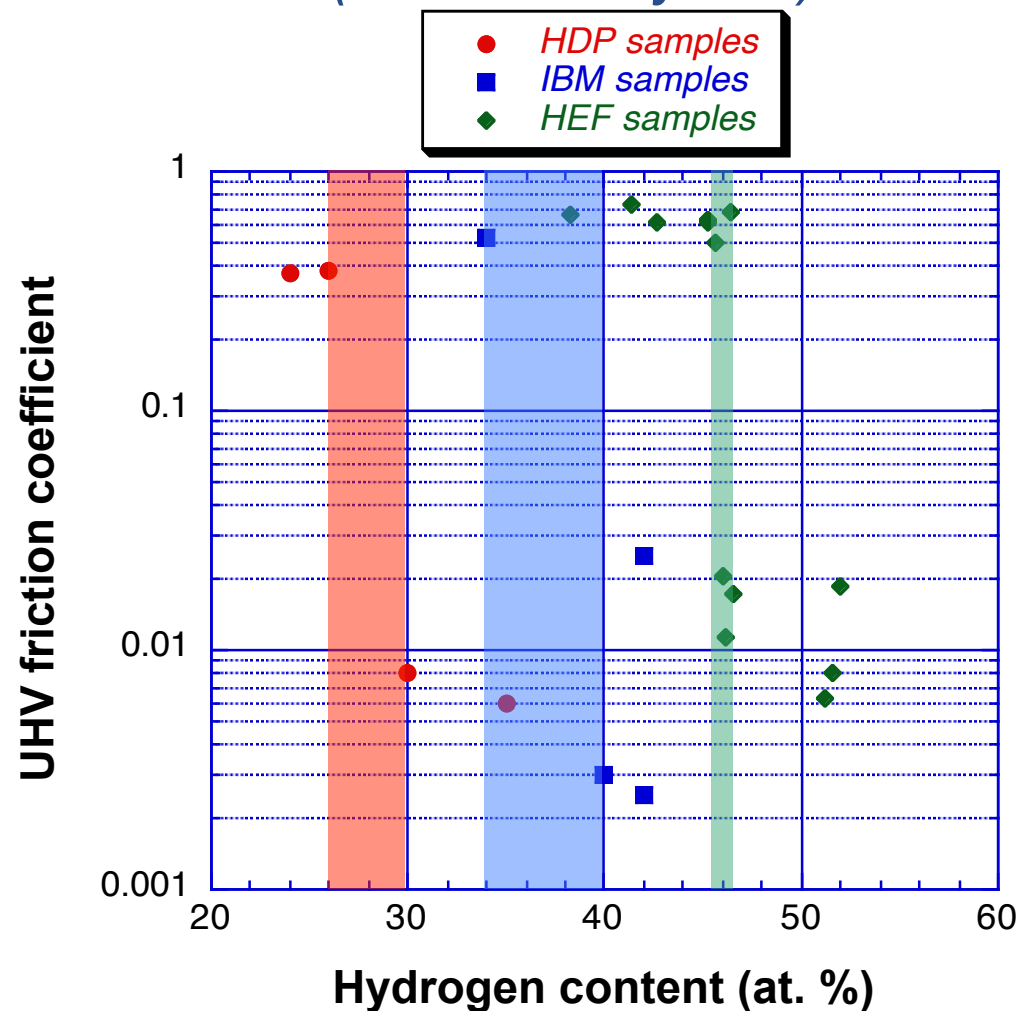


- ▶ Weak interactions between carbon-based sliding surfaces
 - ▶ Reduced adhesion if enough hydrogen on the surface? (or “passivating” species)
 - ▶ Avoiding strong bonds: covalent or metallic

Critical surface coverage by hydrogen?

- **Surface coverage by Hydrogen** would explain superlow friction of a-C:H under ultra-high vacuum?

“Stabilized” UHV friction coefficient
(after 500 cycles)



3 different PECVD processes

HDP: rf-PECVD from $C_2H_2 + H_2$

IBM: dc-PECVD from C_6H_{12} or C_2H_2

HEF: dc-PECVD from C_2H_2
(PVD Ti-based underlayers)

HDP: 26-30 at. %

IBM: 34-40 at. %

HEF: ~ 46 at. %



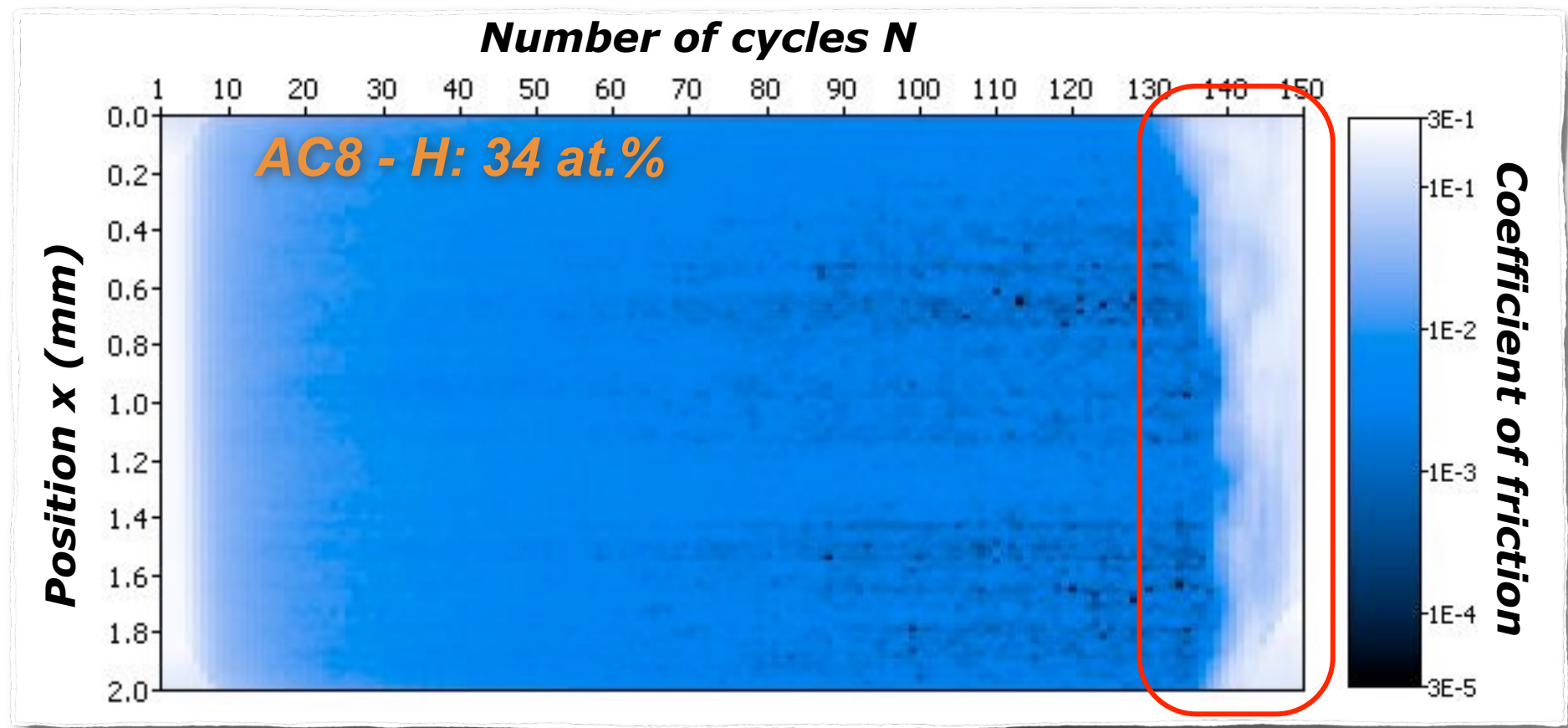
Threshold in hydrogen content
depends on deposition process

*How could we have similar hydrogen coverage
with such different hydrogen contents?*

Loss of superlow friction...

Triboscopy: “friction maps”

Friction as a function of position and number of cycles



Loss of “superlow” friction:

- ▶ Start at localized points of the wear track
 - ▶ Quickly extends to an entire cycle
- $\Rightarrow$ *due to adhesive phenomena*

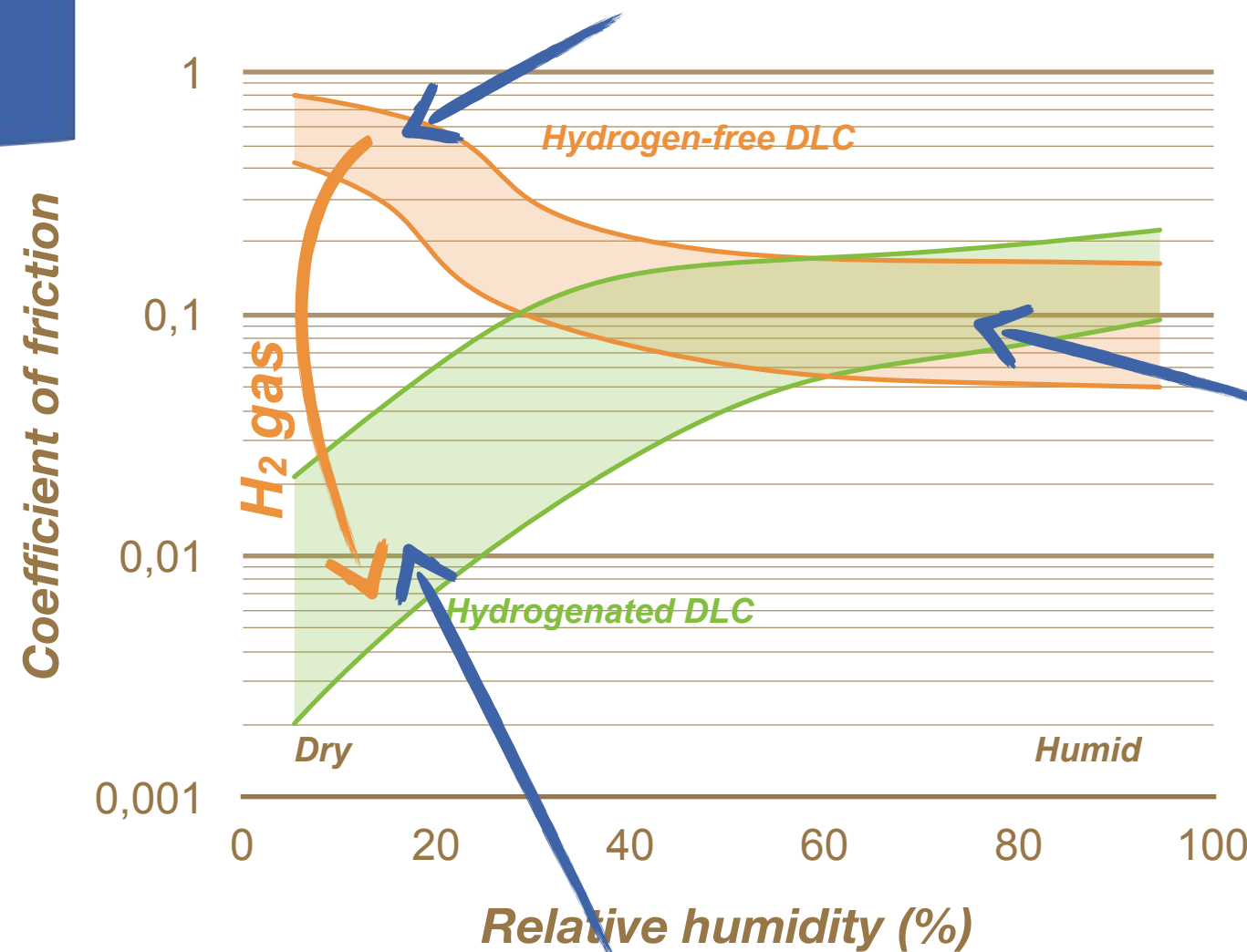
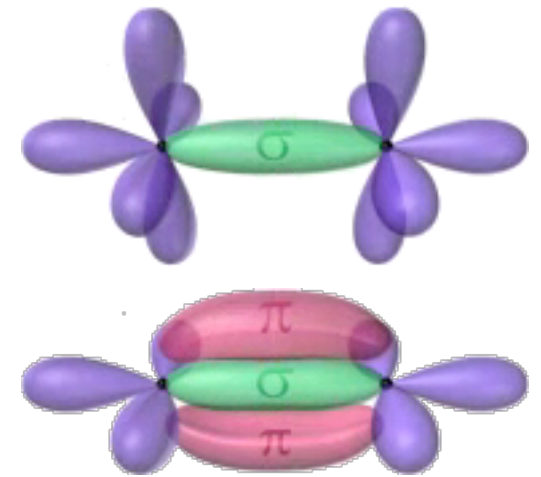
The key-role of adhesive phenomena

- ▶ **Positive role** of adhesive phenomena:
→ promote tribofilm build-up and friction reduction
- ▶ **Negative role** of adhesive phenomena:
→ may lead to drastic friction increase
- ▶ **Adhesion** seem to control the friction of DLC
→ related to surface chemistry?

Surface chemistry & adhesion

Strong adhesion

- ▶ “Dangling” σ bonds
- ▶ π orbitals interactions? Metallic bonding?



Intermediate adhesion

Critical role of water vapor

- ▶ Hydrogen bonding?
- ▶ Capillarity?

Weak adhesion

- ▶ Hydrogen-terminated surfaces
- ▶ Van der Waals interactions

Solid lubrication processes of Diamond-Like Carbon

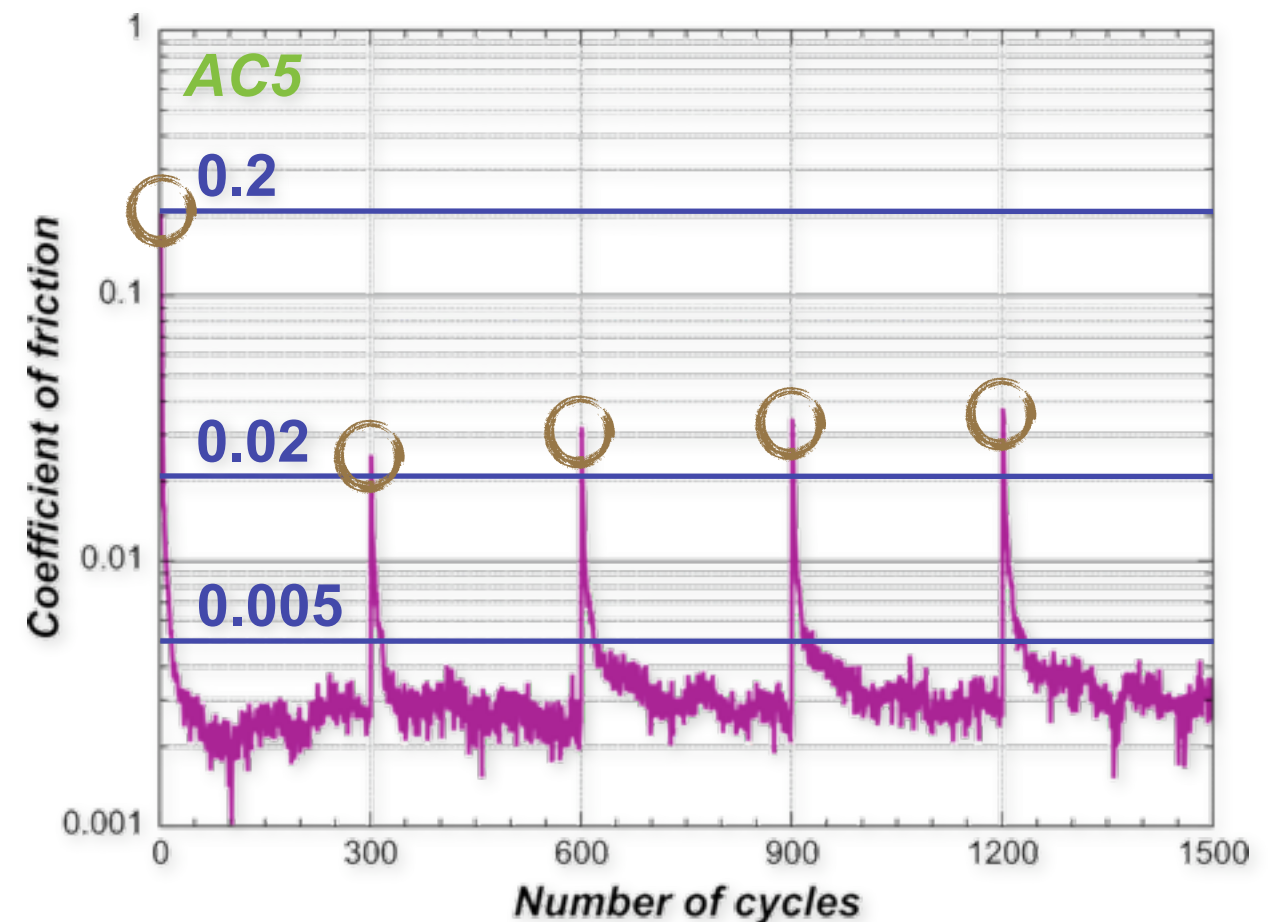
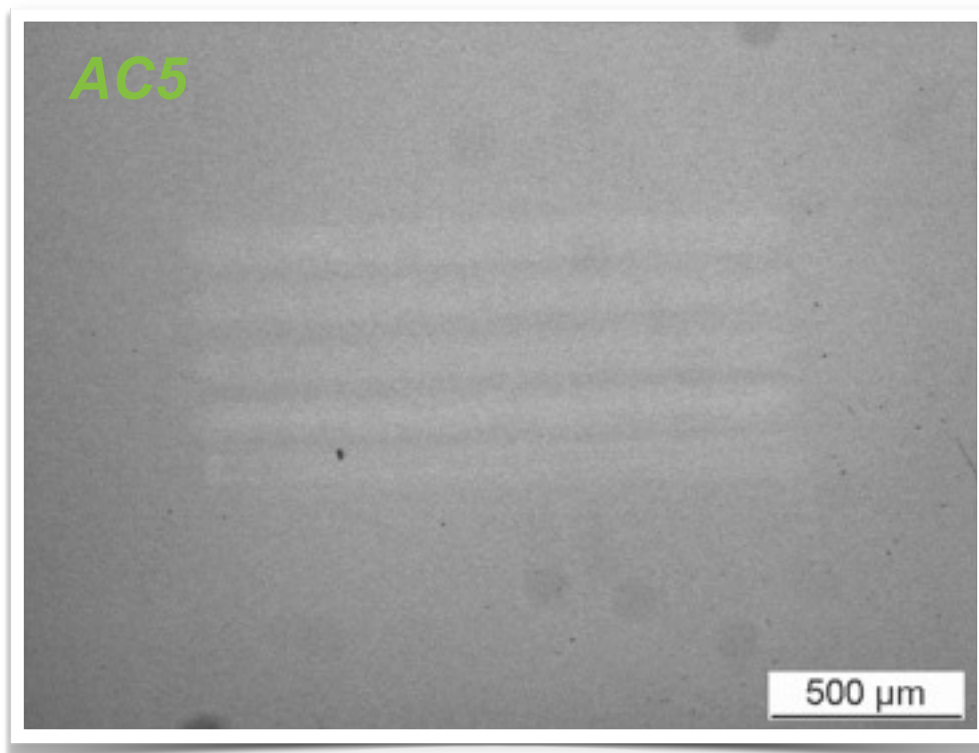
- ▶ Introduction to DLC coatings
- ▶ Role of surface chemistry
- ▶ **Role of surface topography**
- ▶ Interactions with environment
- ▶ Discussion & summary

A closer look at running-in...

Running-in: only due to tribofilm build-up?

UHV friction experiments with :

- ▶ 5 different positions on the DLC coated flat
- ▶ Same position on the steel pin
- ▶ 300 cycles at each flat position



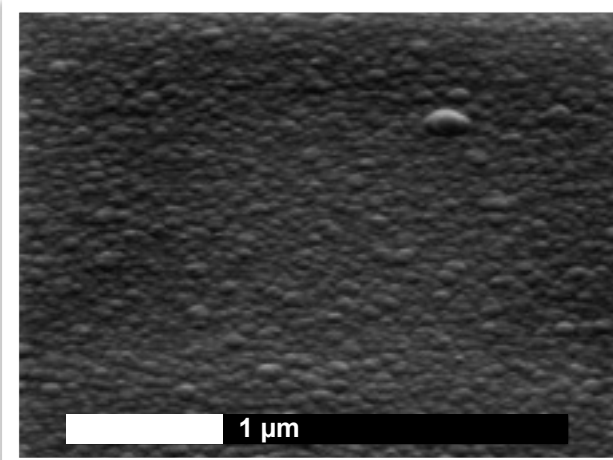
Systematic running-in from > 0.02 during > 15 cycles...
Something has to change on DLC surface!

Investigating surface morphology

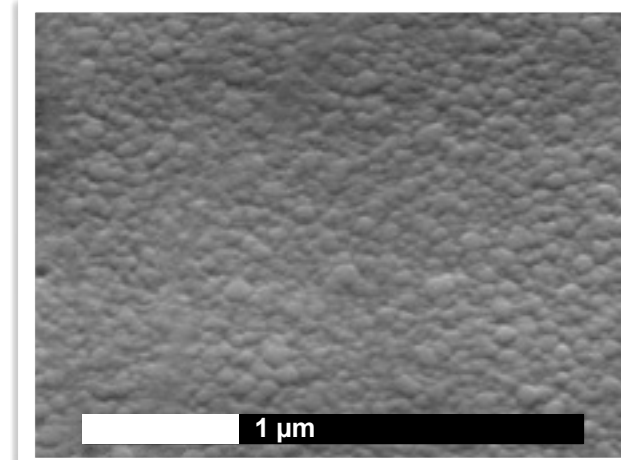
AC5
0 cycles

$R_a = 2.7 \text{ nm}$
 $R_q = 3.4 \text{ nm}$

$\mu \approx 0.25$



Before friction



Superlow friction

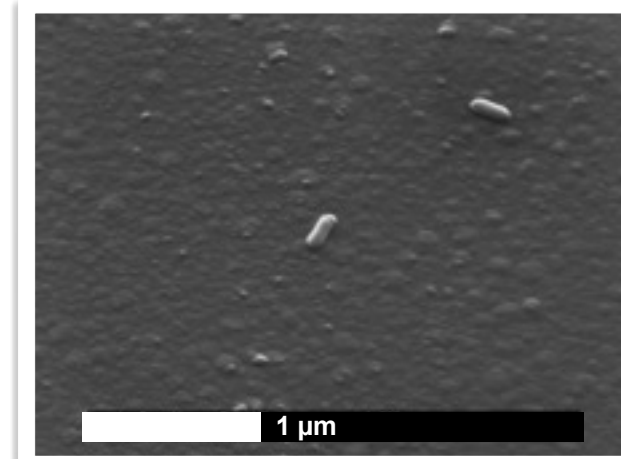
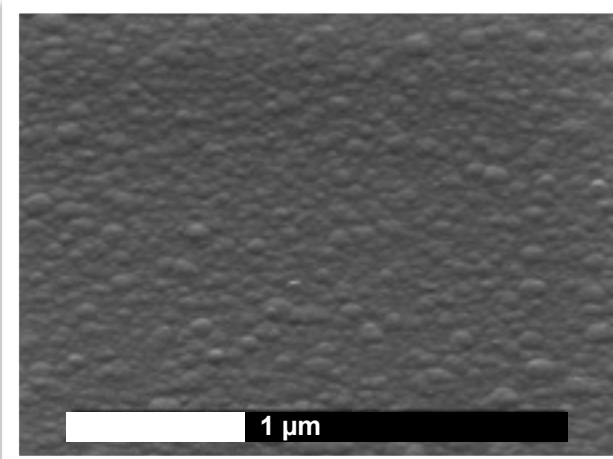
AC5
500 cycles

$R_a = 1.4 \text{ nm}$
 $R_q = 1.9 \text{ nm}$

$\mu \approx 0.003$

AC8
0 cycles

$R_a = 1.8 \text{ nm}$
 $R_q = 2.4 \text{ nm}$



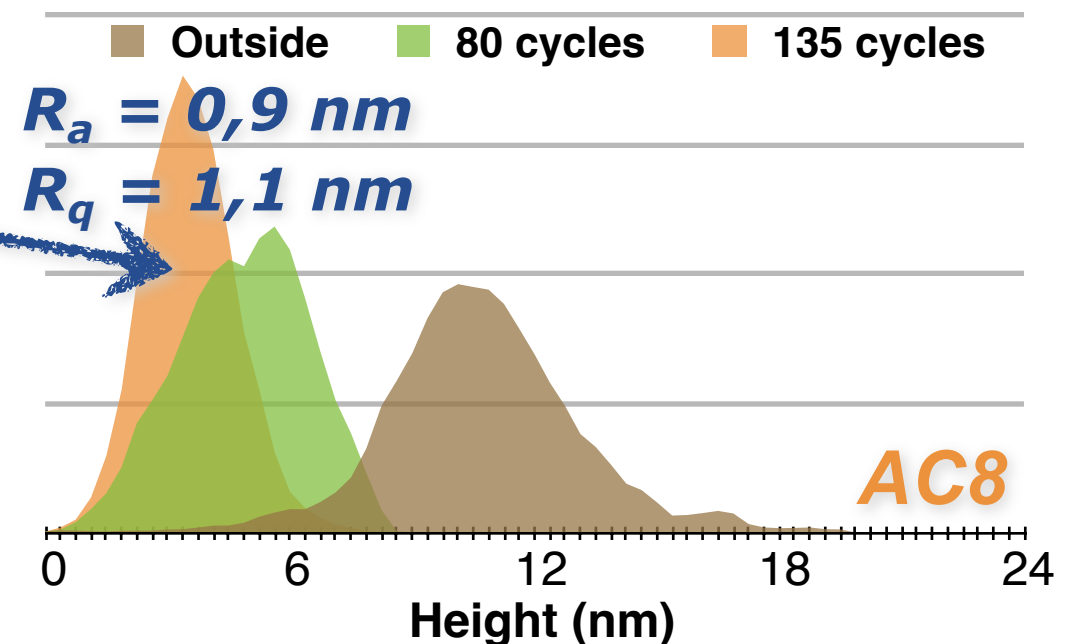
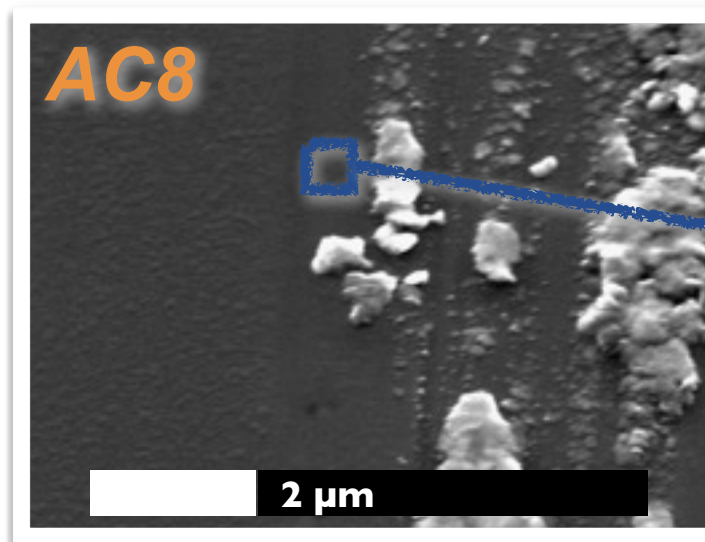
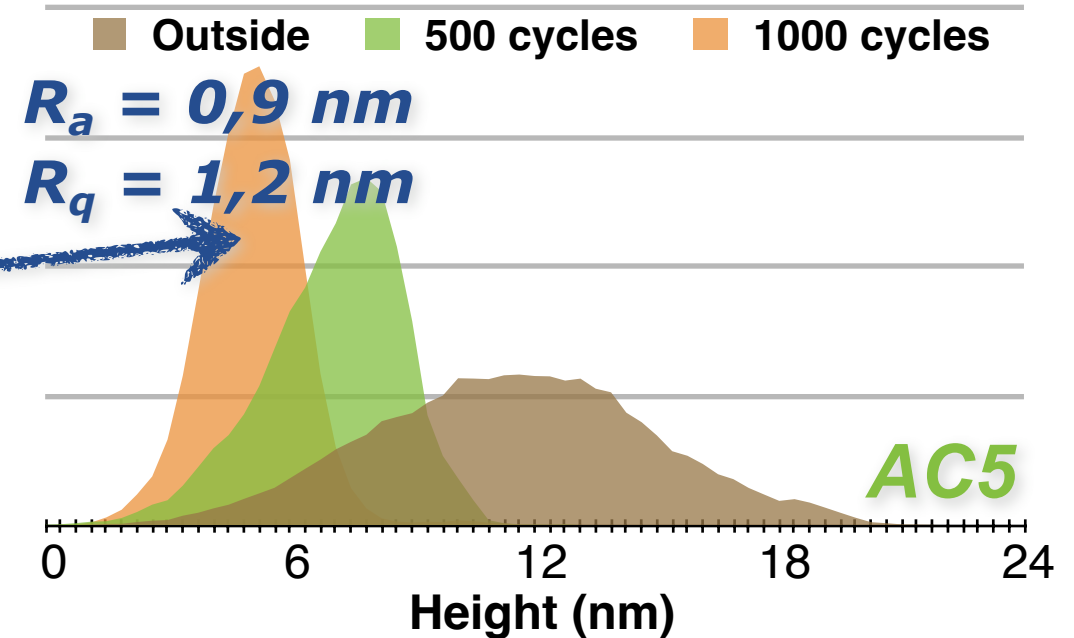
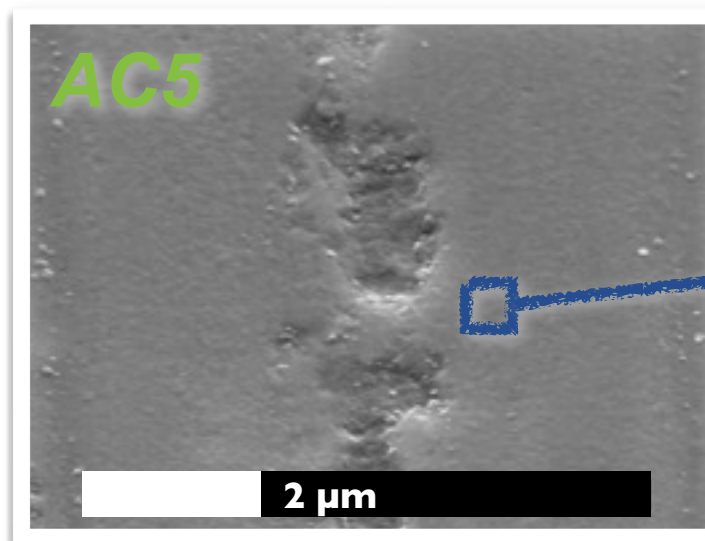
AC8
80 cycles

$R_a = 1.3 \text{ nm}$
 $R_q = 1.6 \text{ nm}$

- ▶ Topography observed by SEM and measured by AFM
- ▶ Both samples exhibit **roughness at nanoscale**
- ▶ Partial wear of asperities is necessary to reach superlow friction
- ▶ Wear of **AC8** asperities seems faster than **AC5**

Surface smoothing & adhesion

What happens near the high friction areas?



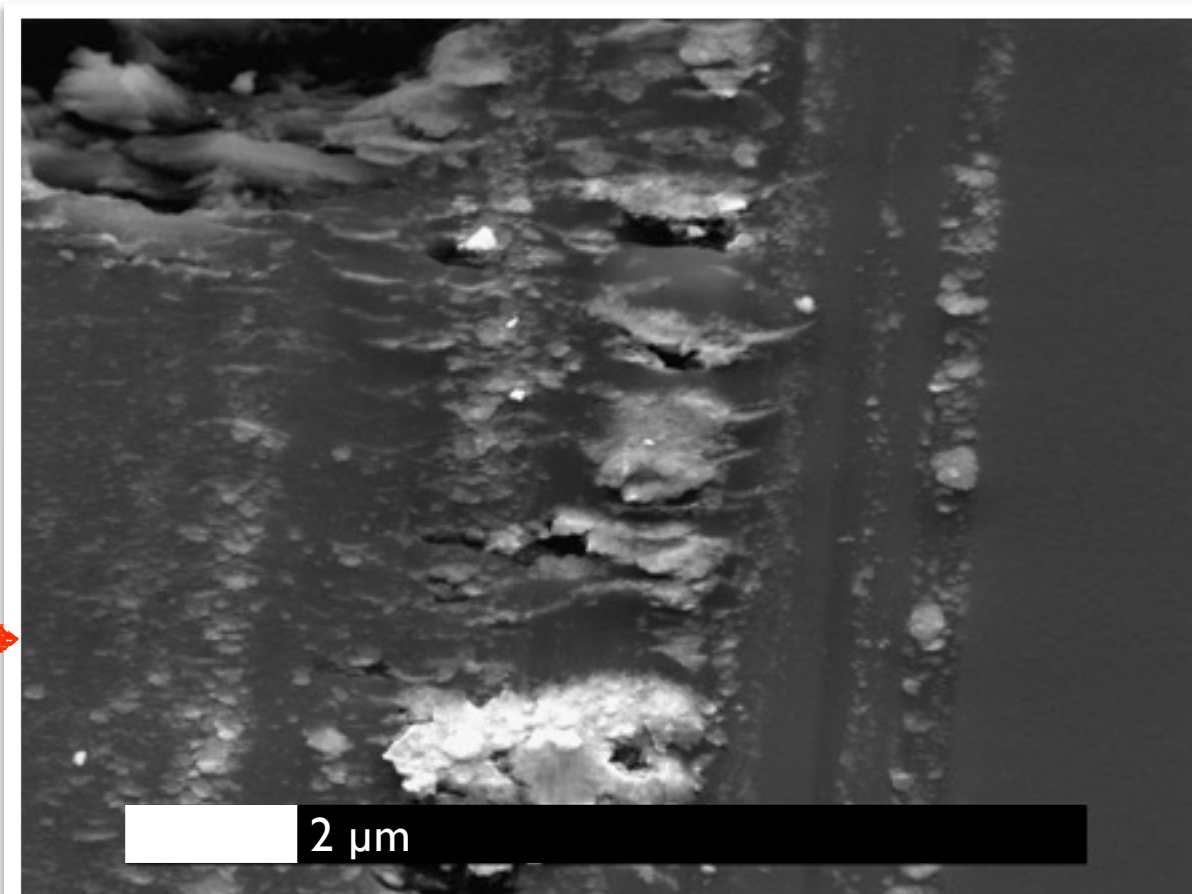
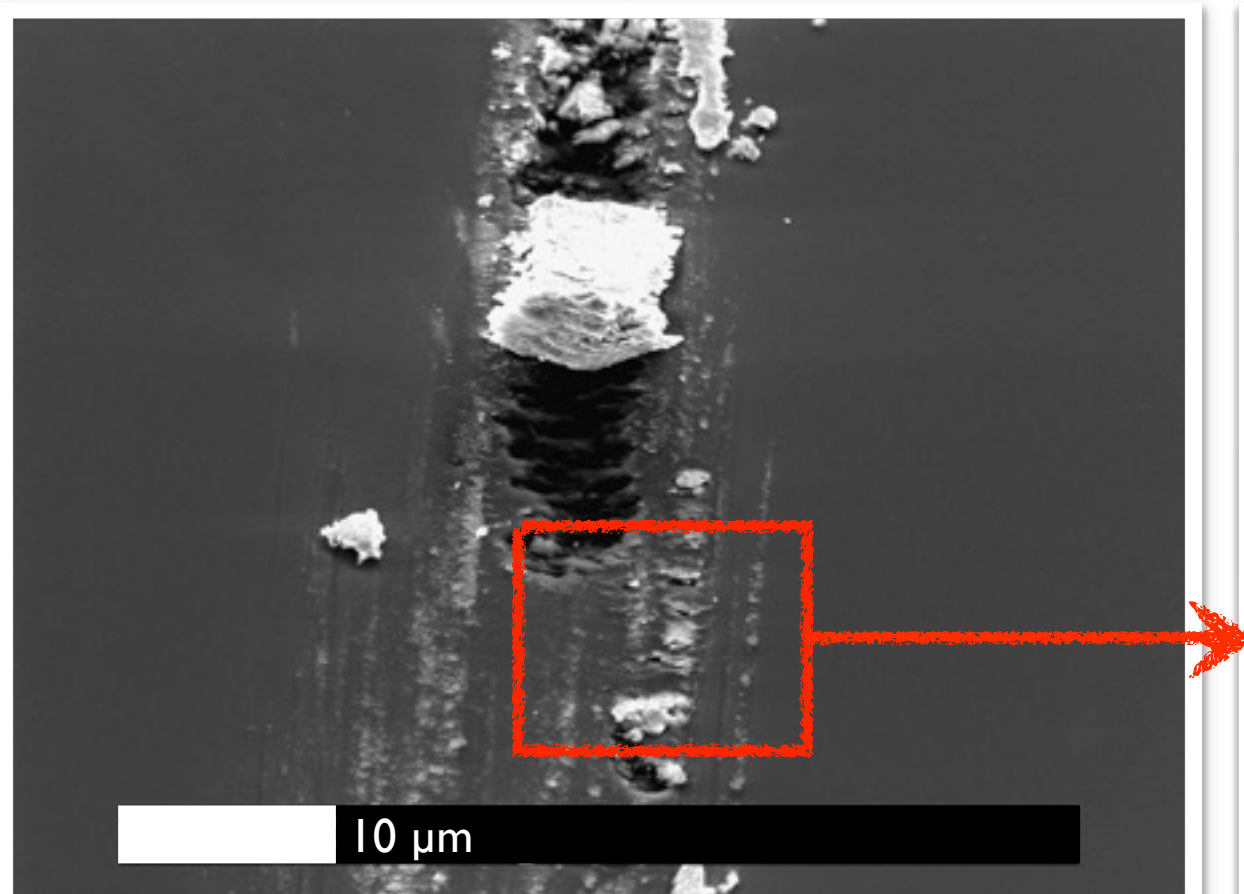
*Smoothing of nanoscale roughness leads to **large adhesive phenomena***

Why such different friction evolution between these two coatings?

Consequences of adhesion

SEM / EDX observations of wear tracks on the AC8 flat:

- ▶ *Iron is transferred to the DLC surface (in high friction zones)*
- ▶ *Some cracks can be found in the DLC around transferred iron particles*
- ▶ *Deep grooves are then formed from these “adhesive junctions”*
- ▶ *Adhesion is clearly controlling the loss of superlow friction for AC8*

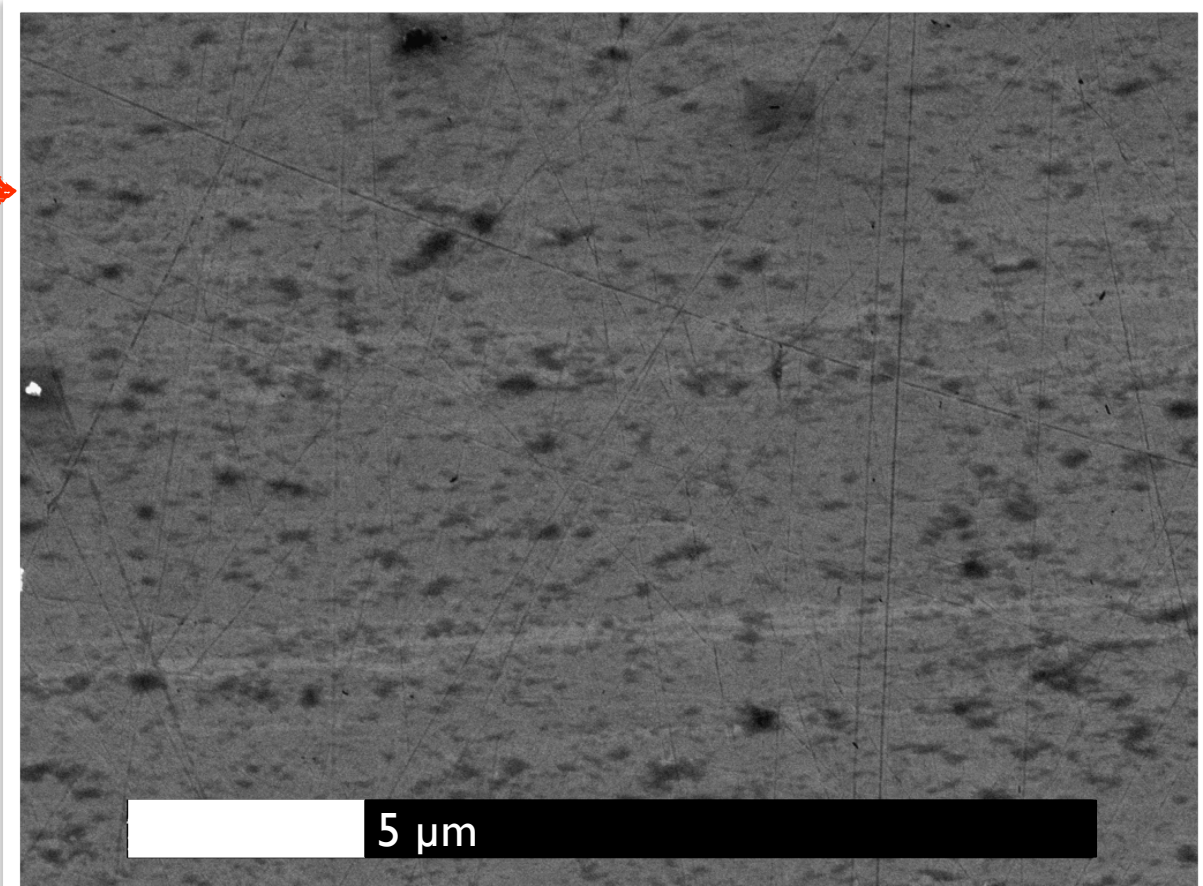
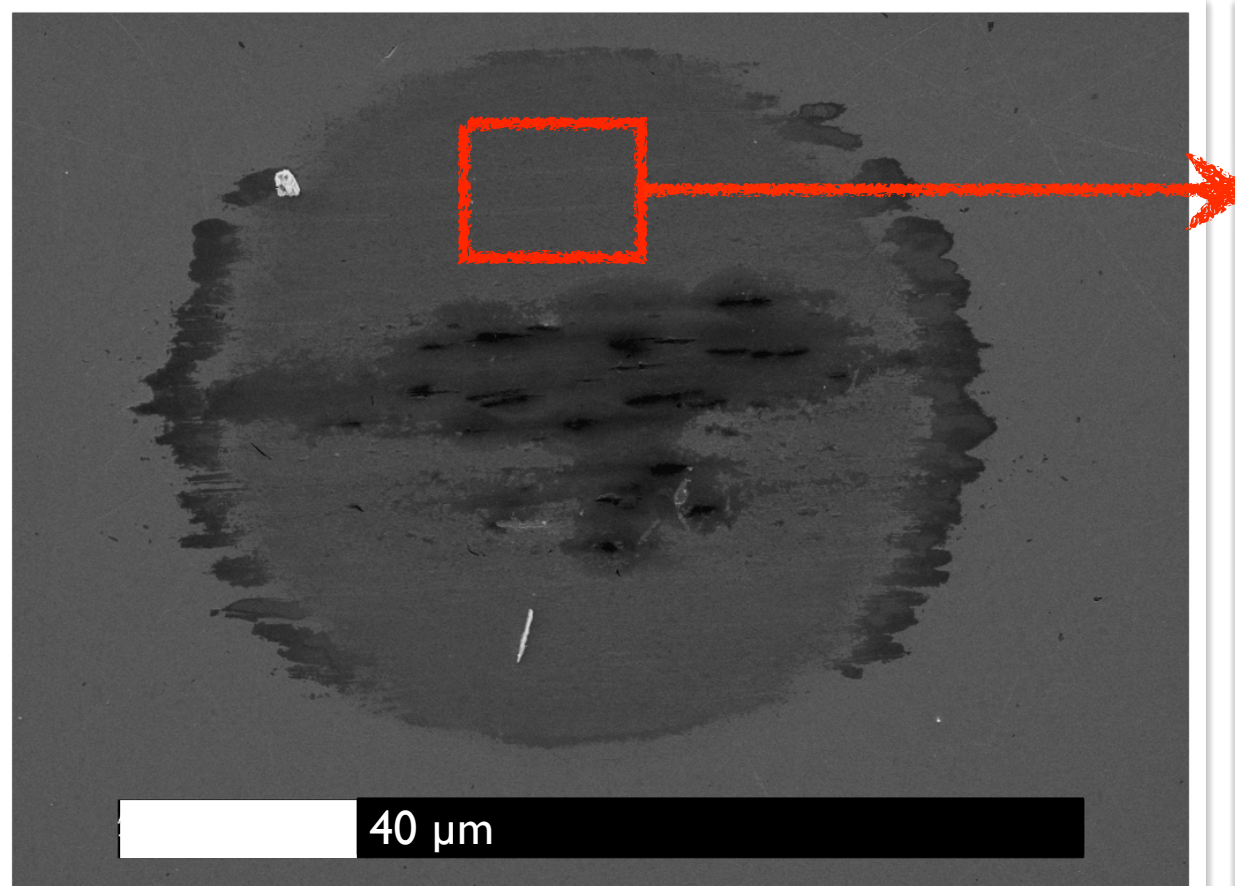


AC8 - 34 at.% H

Consequences of adhesion

SEM / EDX observations of tribofilm on counterface of AC5:

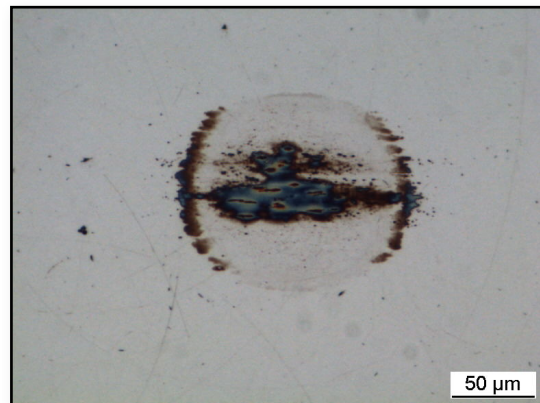
- ▶ *Tribofilm doesn't appear to be continuous!*
- ▶ *Many "dots" of carbon-based materials are covering the steel surface*
- ▶ *Much thicker tribofilm is found in high friction areas*
- ▶ *Growth of tribofilm results from the release of adhesive junctions*



AC5 - 40 at.% H

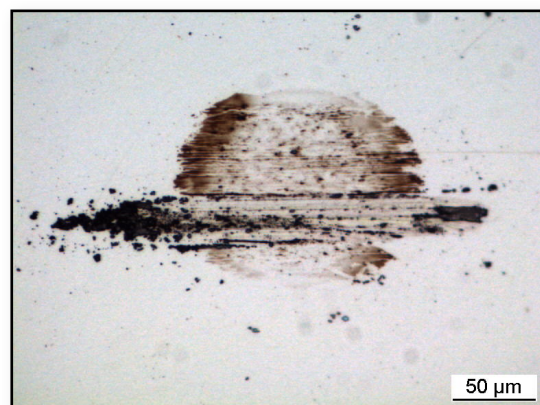
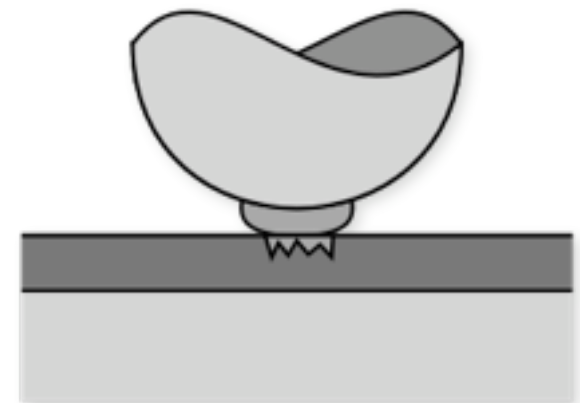
Key-role of mechanical properties

Mechanical properties of DLC control how adhesive junctions will break :



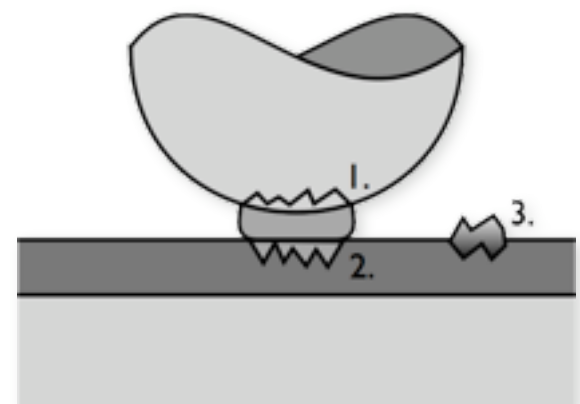
SOFTER AC5 :
 $H = 7.5 \text{ GPa}$
 Viscoplasticity: $6.8 \cdot 10^{-2}$

Adhesion
 ↓
 Transfer of DLC to steel pin
thicker tribofilm
 ↓
 Preserving **low friction**

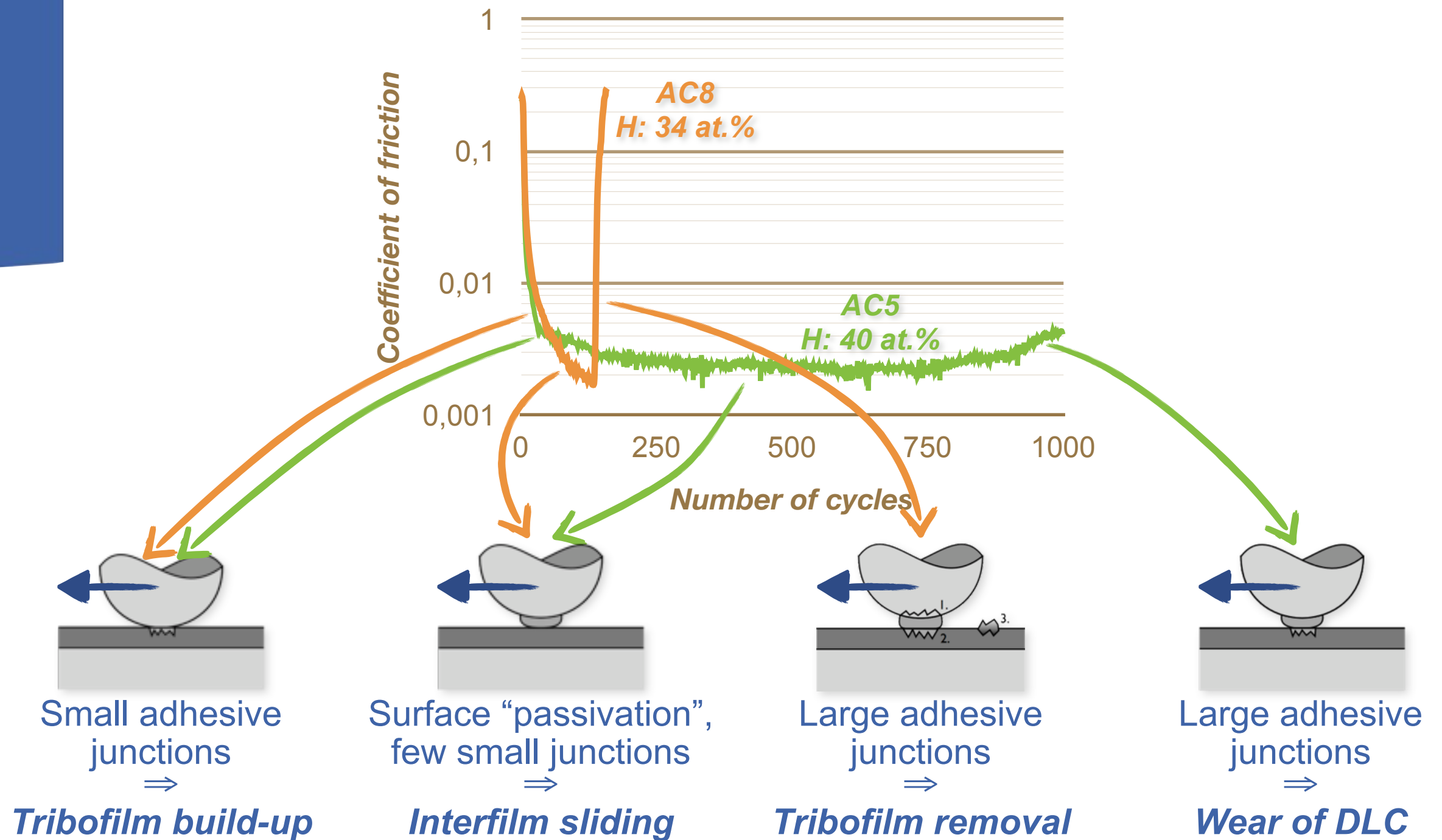


HARDER AC8 :
 $H = 10.5 \text{ GPa}$
 Viscoplasticity: $1.4 \cdot 10^{-2}$

Adhesion
 ↓
 Transfer of steel to DLC flat
Tribofilm removal
 ↓
 Leading to **high friction**



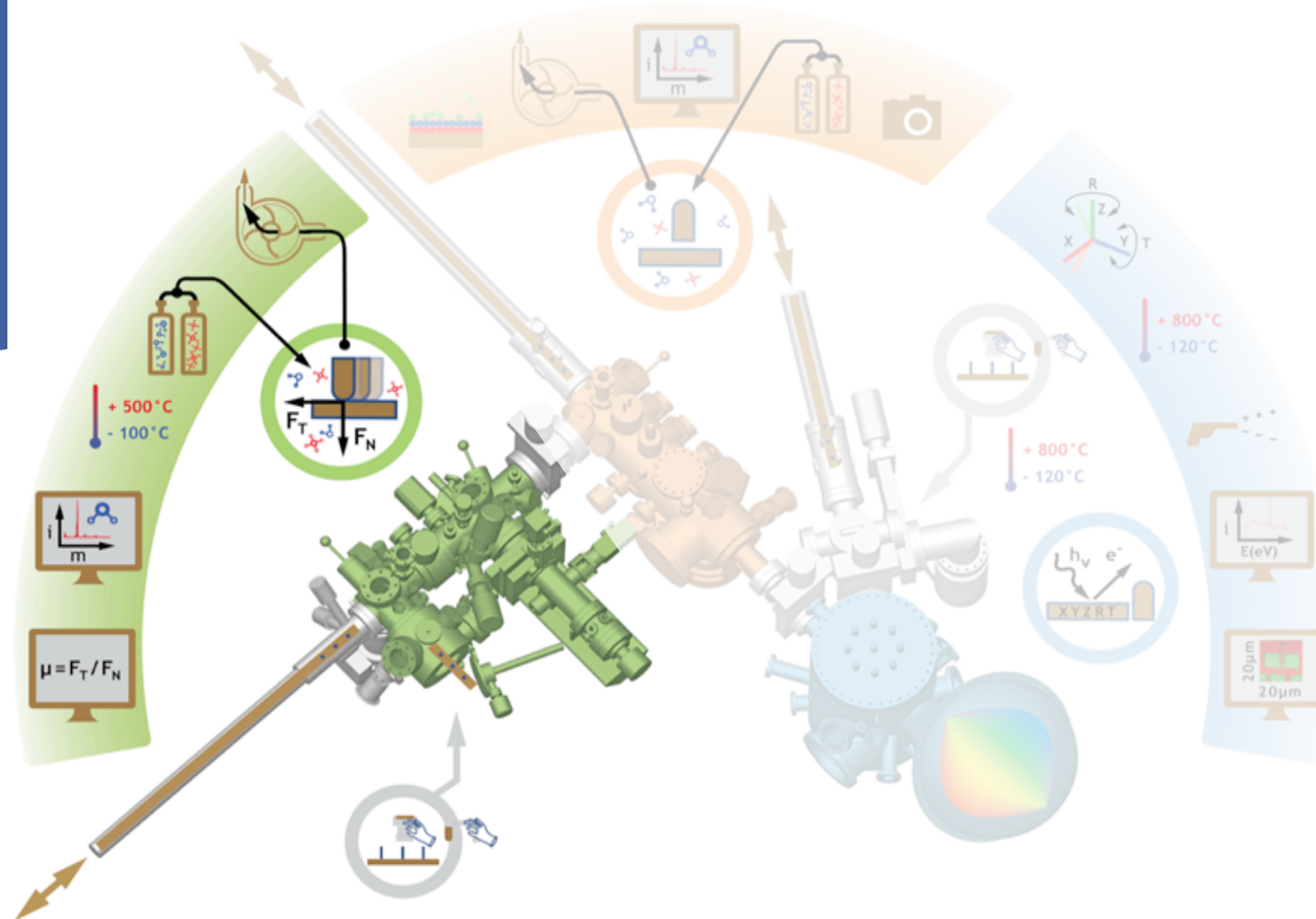
Solid lubrication process of DLC



Solid lubrication processes of Diamond-Like Carbon

- ▶ Introduction to DLC coatings
- ▶ Role of surface chemistry
- ▶ Role of surface topography
- ▶ **Interactions with environment**
- ▶ Discussion & summary

Environment-controlled experiments on $\text{SiO}_x\text{-DLC}$



***Si wafer coated
with a-C:H:Si:O***

C: 57 ± 3 at.% H: 34 ± 3 at.%
Si: 6 ± 1 at.% O: 3 ± 1 at.%

Fraction of sp^2 -bonded C:
 $54 \pm 2\%$ (NEXAFS)

Thickness: 1.9 ± 0.1 μm
Roughness (rms): 1.4 ± 0.1 nm
(over $5 \times 5 \mu\text{m}^2$)
H = 10 GPa – $E^* = 140$ GPa

Experimental conditions

Materials: **Steel pin, Si-coated flat**
Experiments under O_2 :

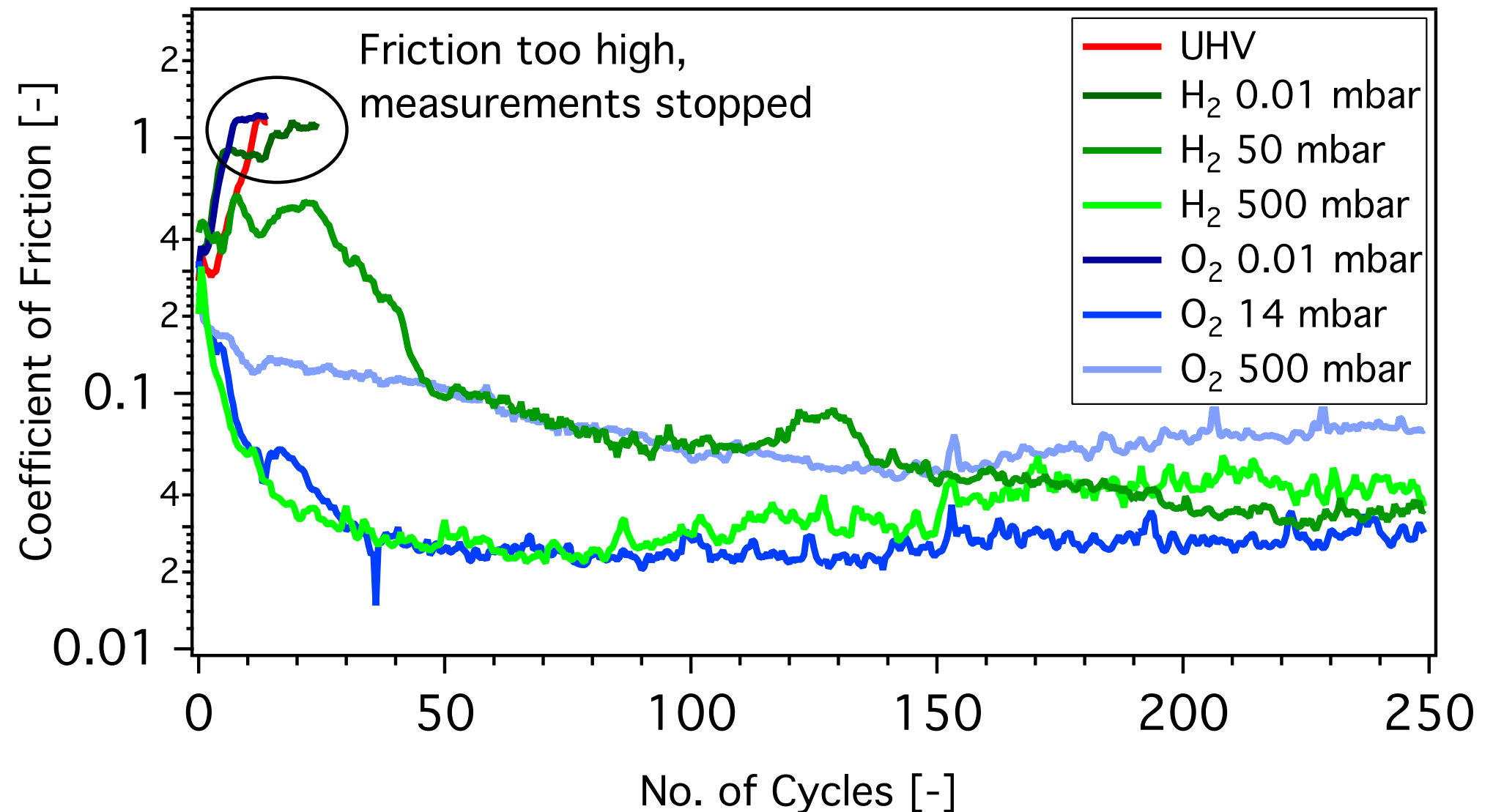
0.01 mbar up to 1000 mbar

Experiments under H_2 :

0.01 mbar up to 2000 mbar

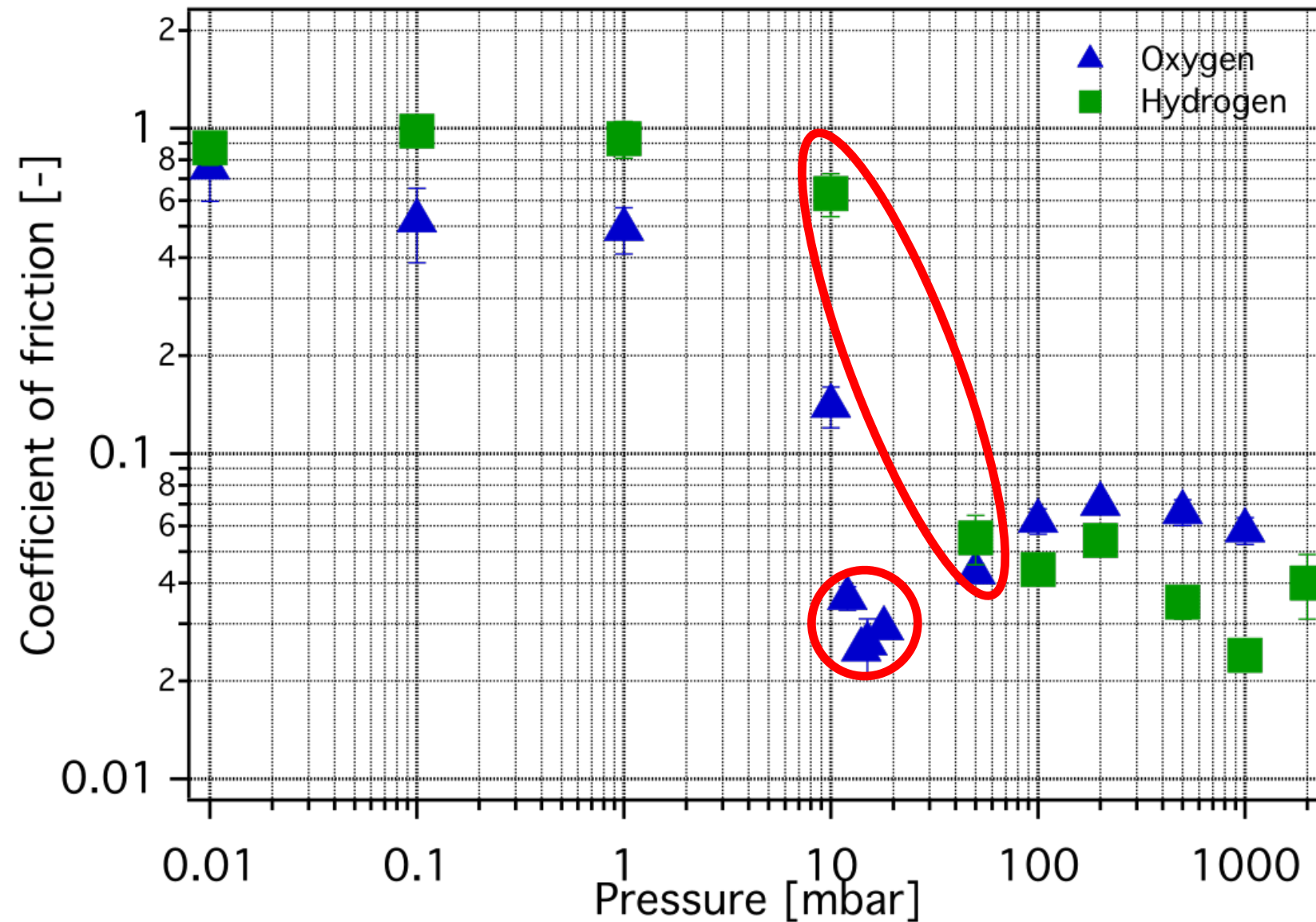
Pin diameter: 8 mm
Sliding Speed: 0.5 mm/s
Applied load: 3 N (≈ 430 MPa)
Track's length: 2 mm

Friction evolution in H_2 & O_2



- ▶ HV and low gas pressure: **very high friction**
- ▶ With higher pressures of O_2 or H_2 : **lower friction**
- ▶ Computing an average coefficient of friction

Threshold in gas pressure to achieve low friction



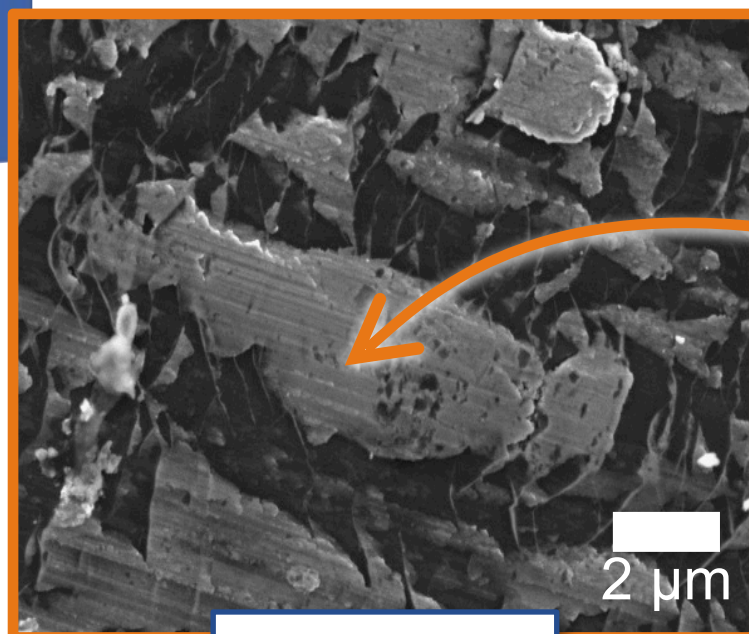
- ▶ Clear **threshold** between high and low friction
- ▶ At least 14 mBar of O₂ or 10 to 50 mBar of H₂ is required

Transfer phenomena triggered by gas pressure

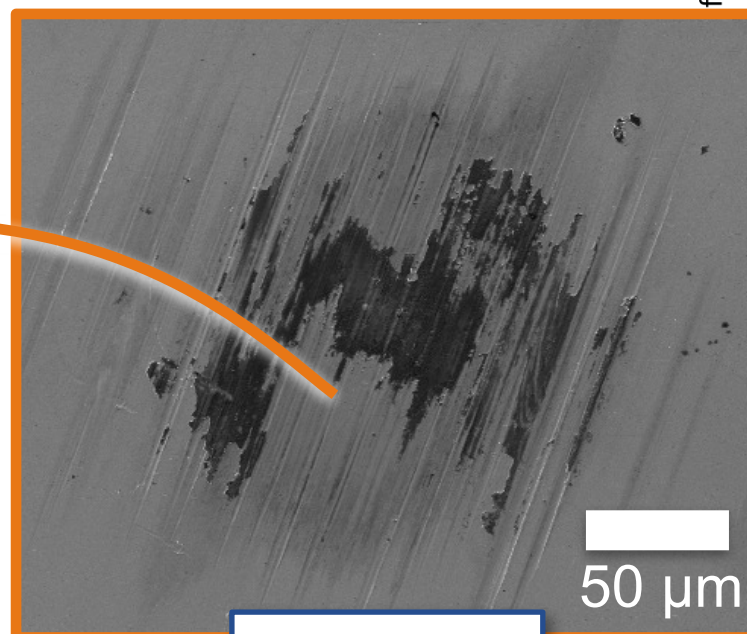
SEM observation of wear tracks

a-C:H:Si:O flat

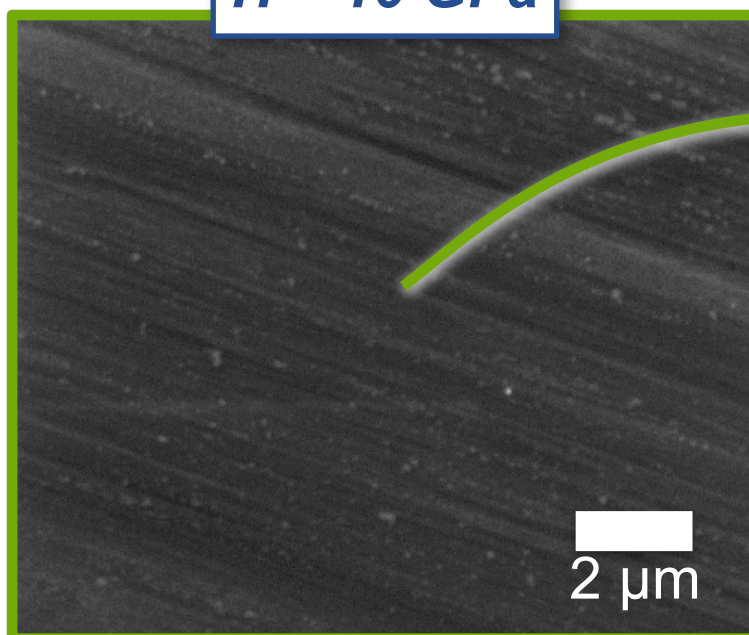
Steel pin



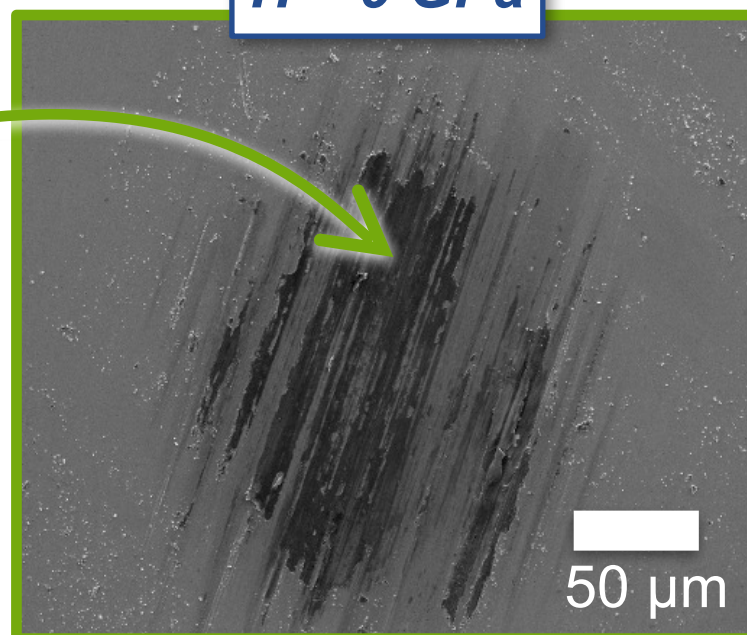
$H = 10 \text{ GPa}$



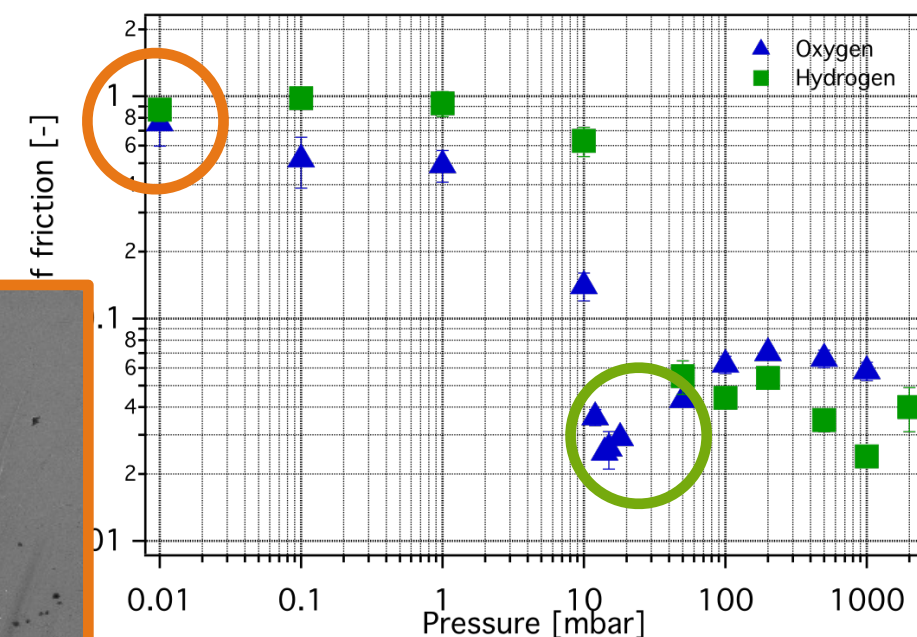
$H = 9 \text{ GPa}$



2 μm



50 μm

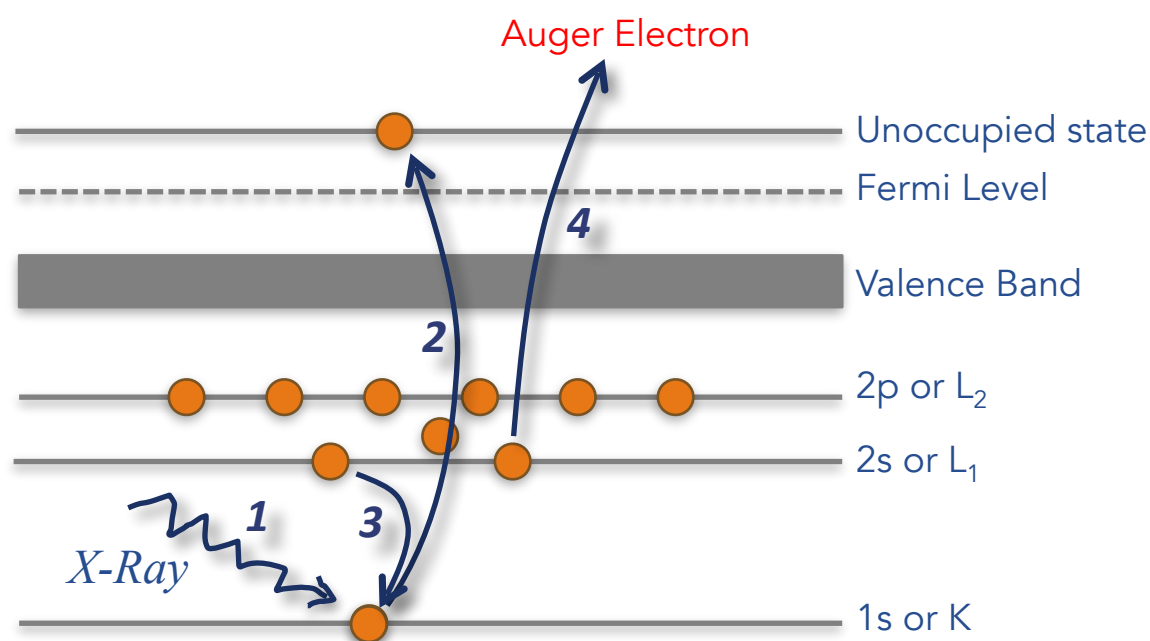


Breakage of adhesive junctions not only controlled by mechanical properties!

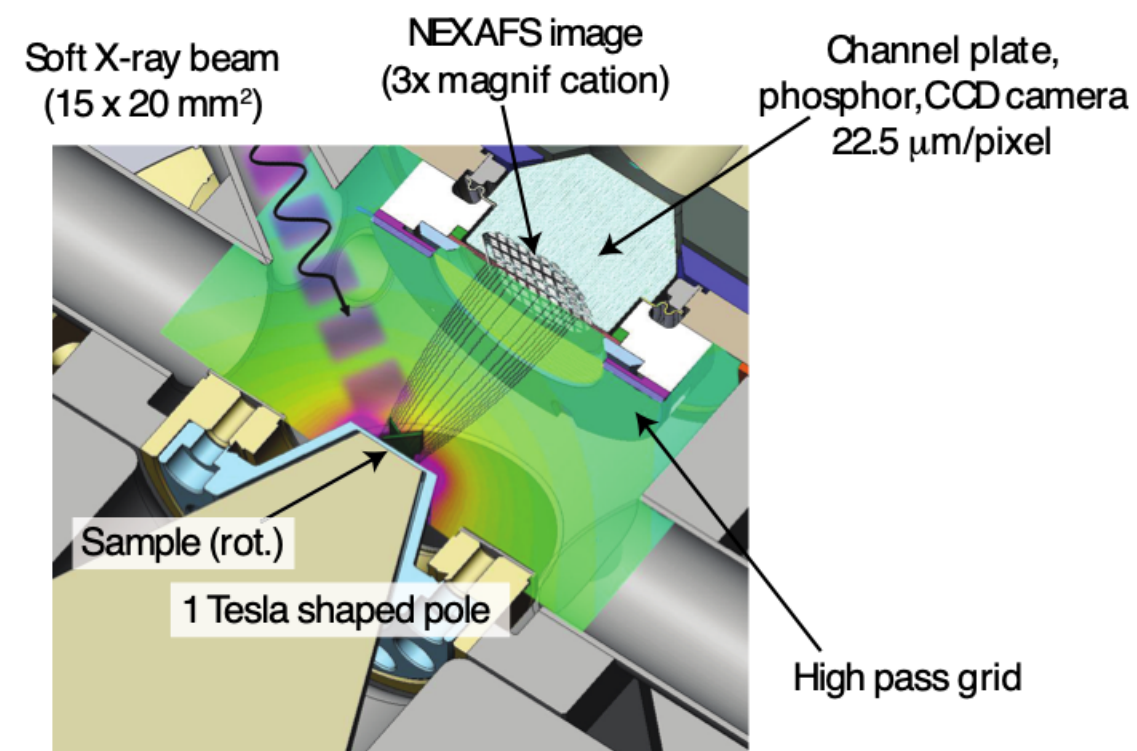
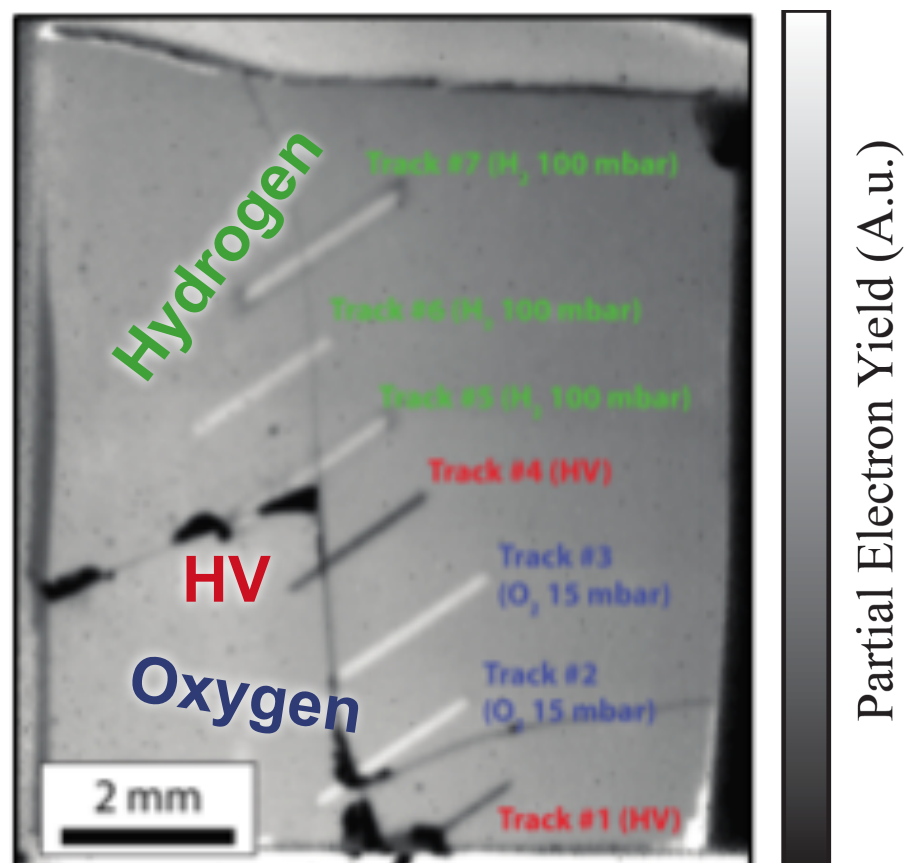
HV and low pressure

High pressure

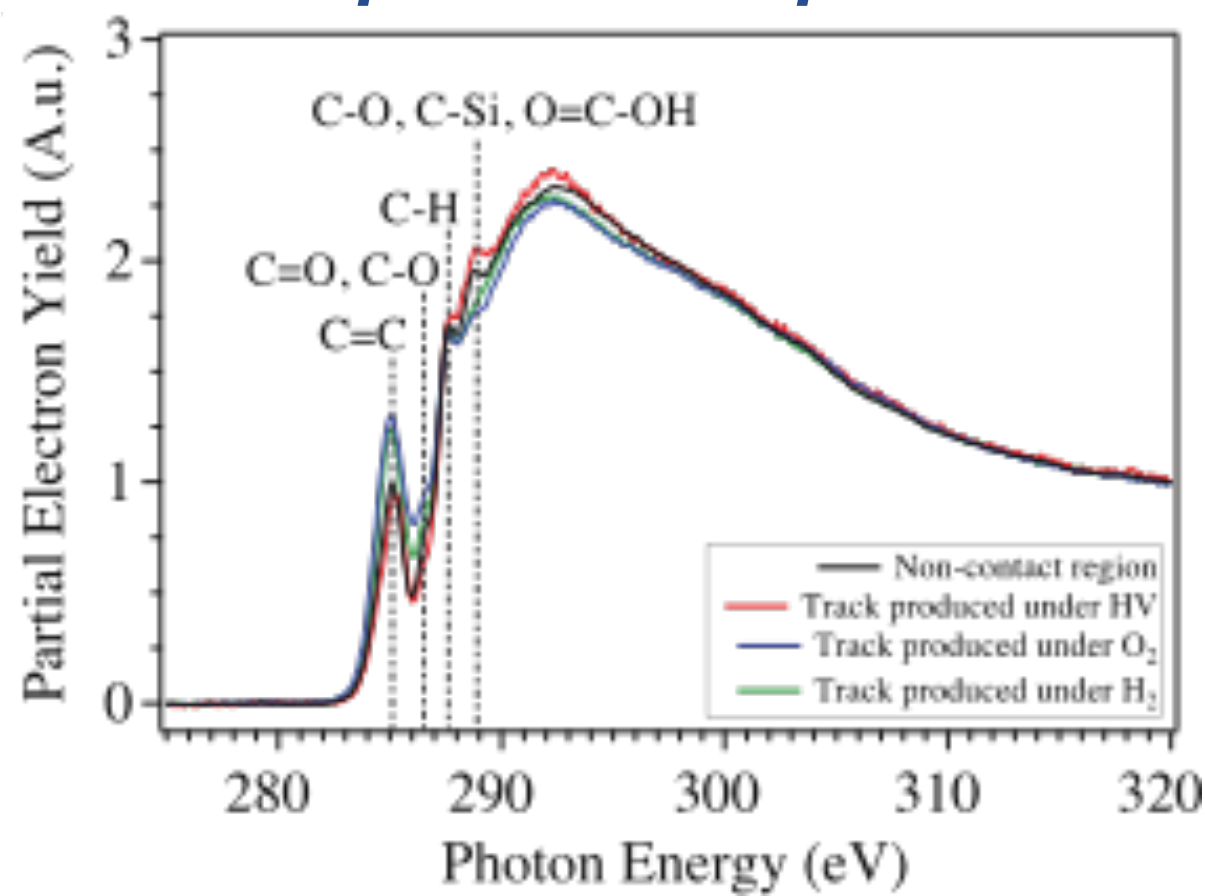
Near-edge X-ray absorption fine structure (NEXAFS)



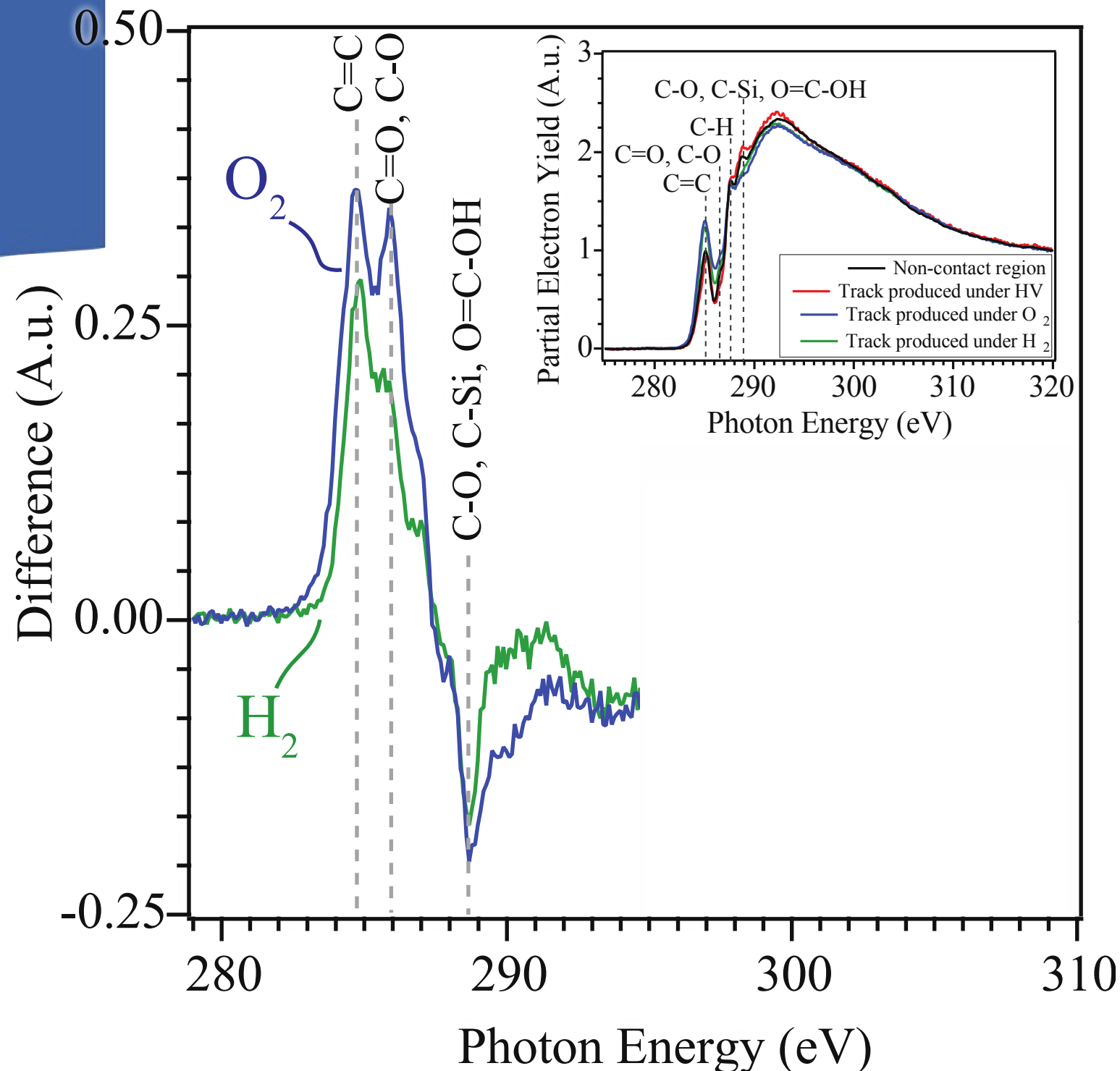
Acquisition of images...



Acquisition of spectra...

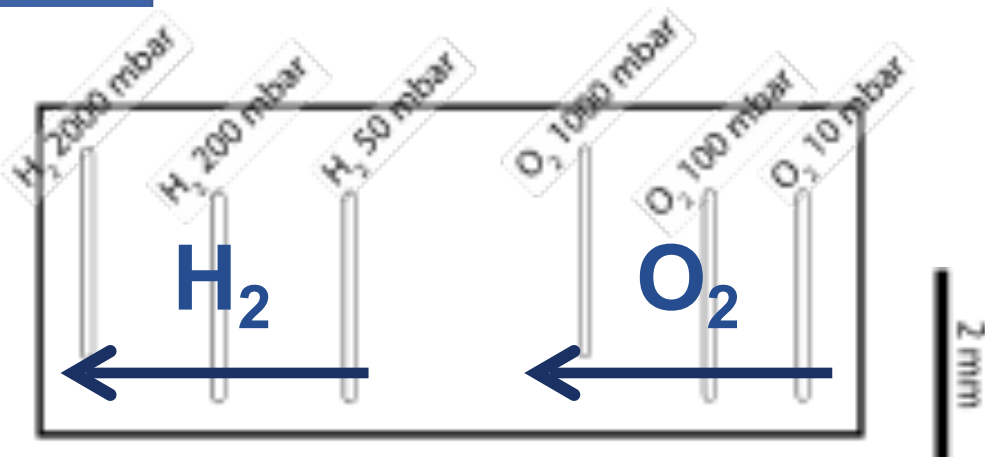


NEXAFS spectra on wear tracks

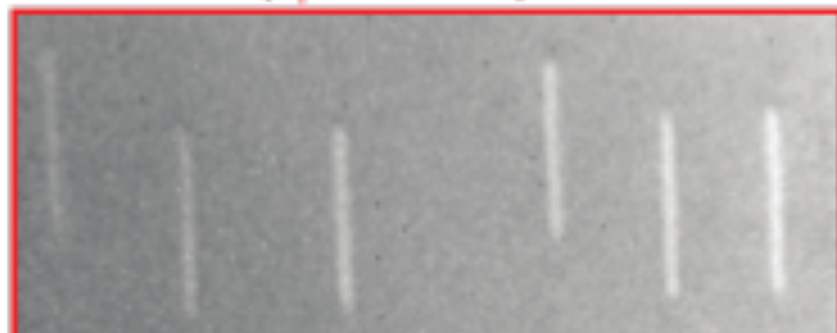


- ▶ Differential spectra by subtracting non-contact region spectrum (remove contribution of adventitious carbon)
- ▶ At 285 eV: strong sp^2 C increase
- ▶ Rehybridization due to C-C bond breaking?

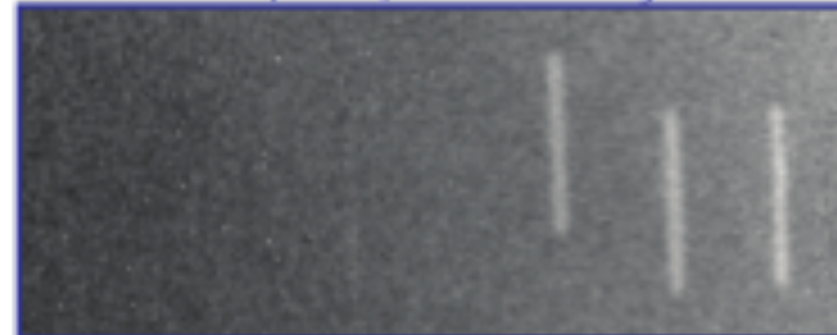
NEXAFS images of wear tracks



$C1s \rightarrow \pi^*$ (sp^2 carbon)



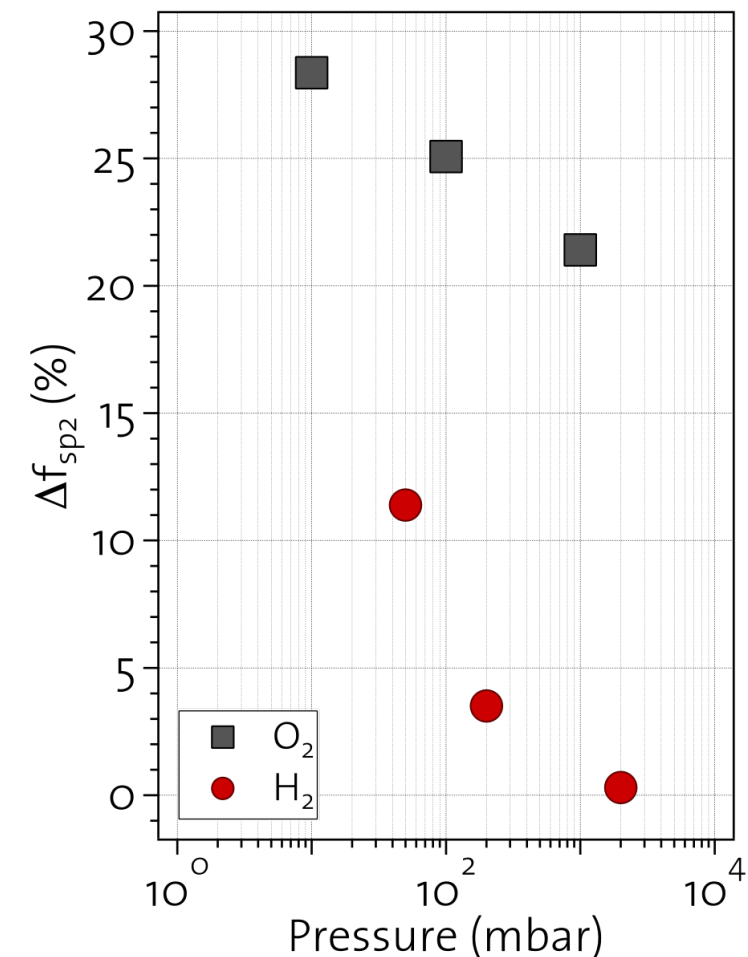
$C1s \rightarrow \pi^*$ ($C=O$) and $C-O$ Ryd. orb.



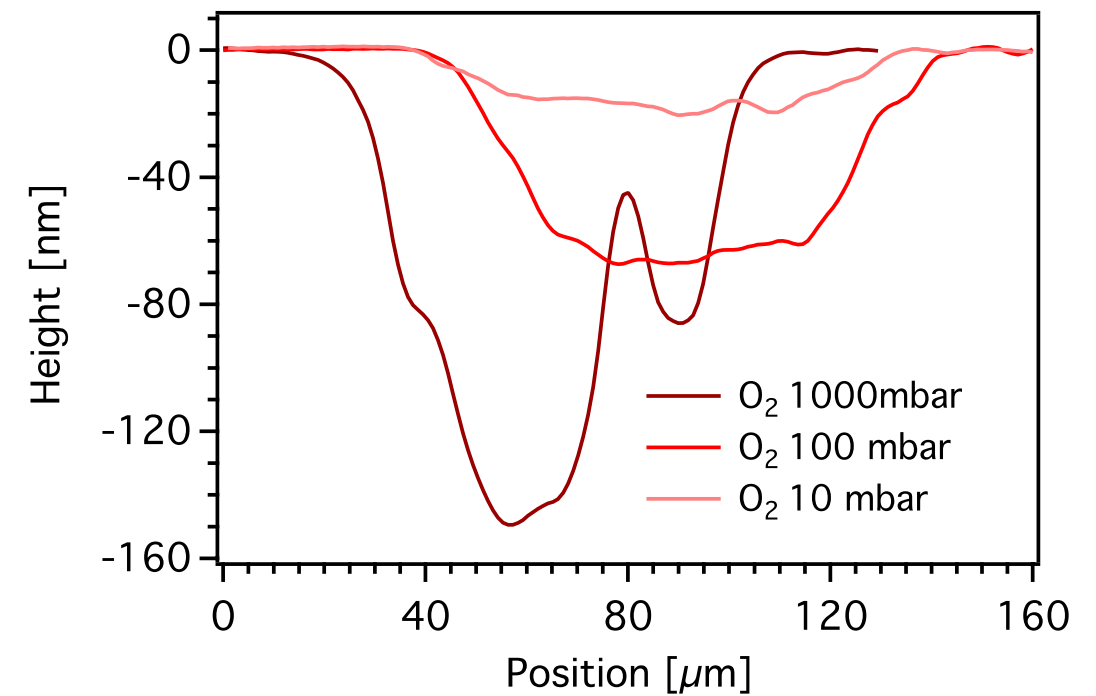
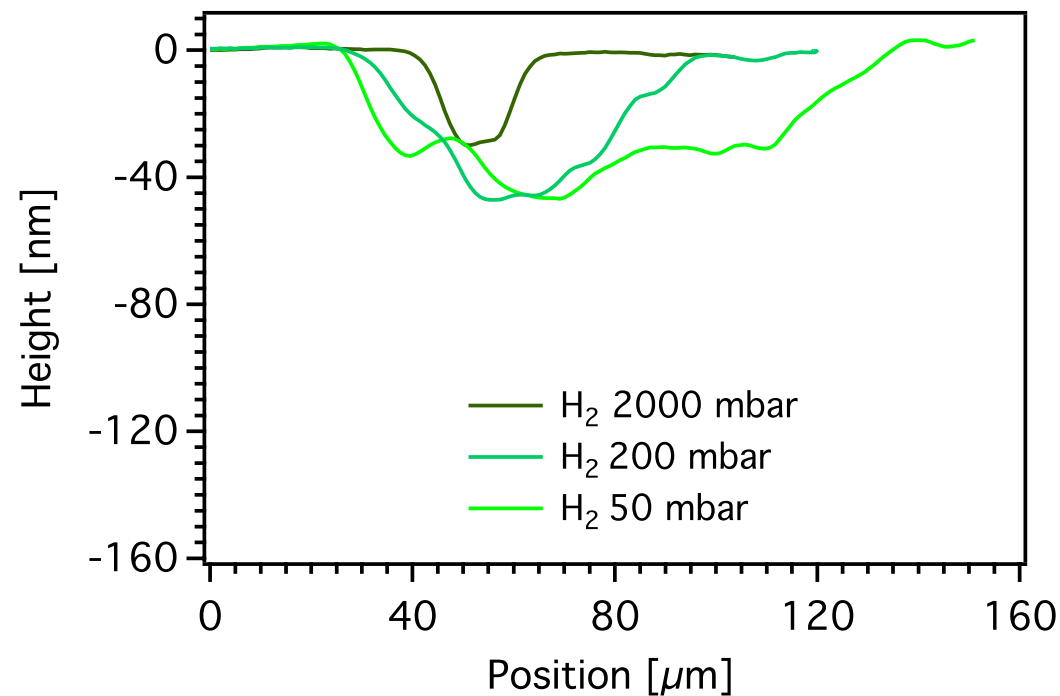
$C1s \rightarrow \sigma^*$ ($C-H$)



- Decreasing sp^2 fraction with increasing gas pressure for both H_2 and O_2
 $\Rightarrow$ rehybridization decreases
- Increasing $C-H$ bonds in H_2 , but slightly decreasing $C-O$ & $C=O$ bonds in O_2
 $\Rightarrow$ surface passivation or not?

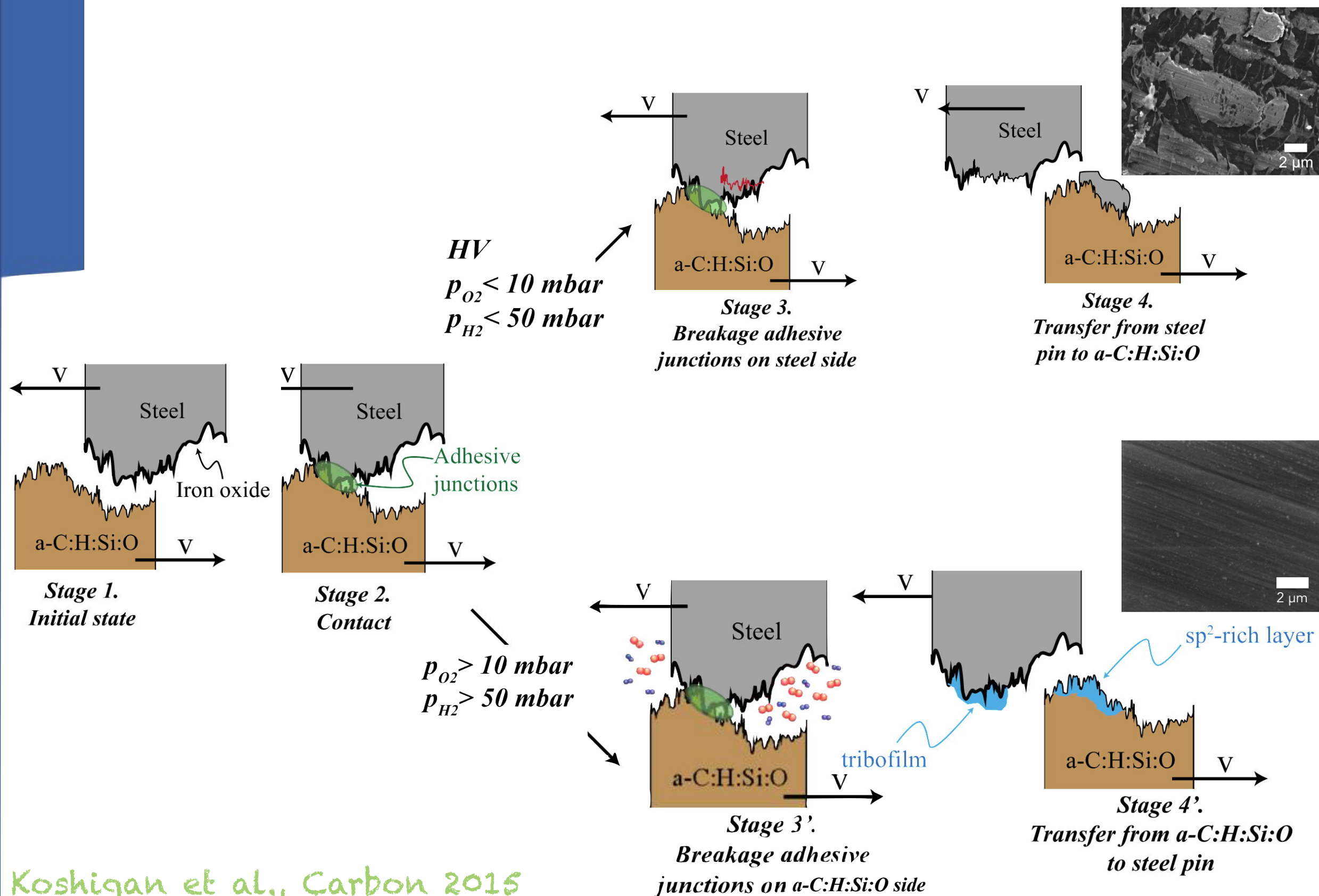


A look at environment effect on wear



- ▶ Just above the threshold, **higher wear in H₂ than in O₂**
- ▶ When increasing gas pressure:
 - ▶ **Wear decreases in H₂**
worn area becomes narrower than contact width!
 - ▶ **Wear increases in O₂**
- ▶ Consistent with less C–C bond breaking in H₂, indeed!
- ▶ For O₂, are volatile species formed (CO, CO₂...)?
Is there a gradient in sp² C near the surface?

A tentative tribological model for a-C:H:Si:O



Solid lubrication processes of Diamond-Like Carbon

- ▶ **Introduction to DLC coatings**
- ▶ **Role of surface chemistry**
- ▶ **Role of surface topography**
- ▶ **Interactions with environment**
- ▶ **Discussion & summary**

Tribology of DLC: multi-physical aspects

Solid lubrication processes of DLC coatings seems to be controlled by:

▶ **Physical interactions**

- ▶ Van der Waals forces (H-terminated surface)
- ▶ Hydrogen bonding (with water vapor)
- ▶ Overlap of π -orbitals (for low H coverage) or even metallic bonding?
- ▶ Physisorption of environmental gases?
- ▶ Contribution of electrostatic interactions?

▶ **Chemical reactions**

- ▶ Covalent bonding between sliding surfaces
- ▶ “Passivation” of dangling bonds by environmental gases
- ▶ Controls the nature of sliding surfaces...

▶ **Surface mechanical behavior**

- ▶ Controls the real area of contact
- ▶ Controls the release of adhesive junctions
- ▶ **Not only hardness** to be considered: viscoplasticity, fracture toughness...
- ▶ Role of time-dependance of mechanical properties?
- ▶ Importance of ductile/brittle transition?

Tribology of DLC: multi-scale aspects

Solid lubrication processes of DLC coatings take place at different scales:

▶ **At the scale of molecules...**

- ▶ Adhesive phenomena are controlled by physical interactions & chemical reactions

▶ **At the scale of asperities...**

- ▶ Nanoscale surface topography controls the size of adhesive junctions
- ▶ Mechanical behavior of asperities controls friction & wear

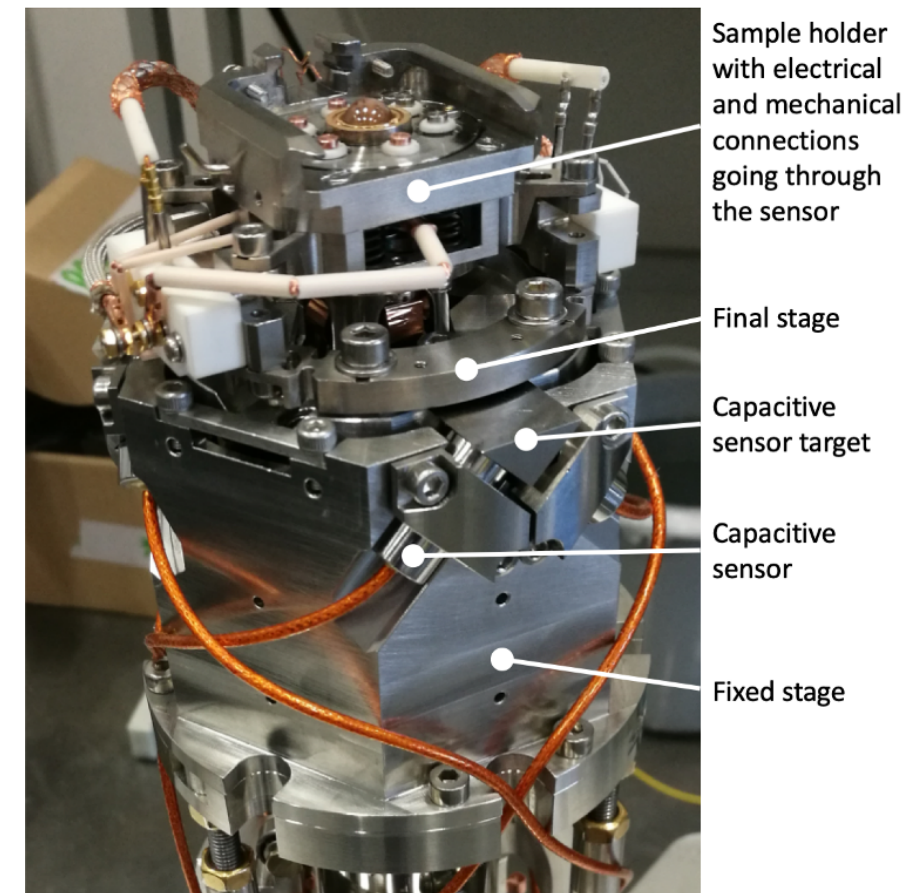
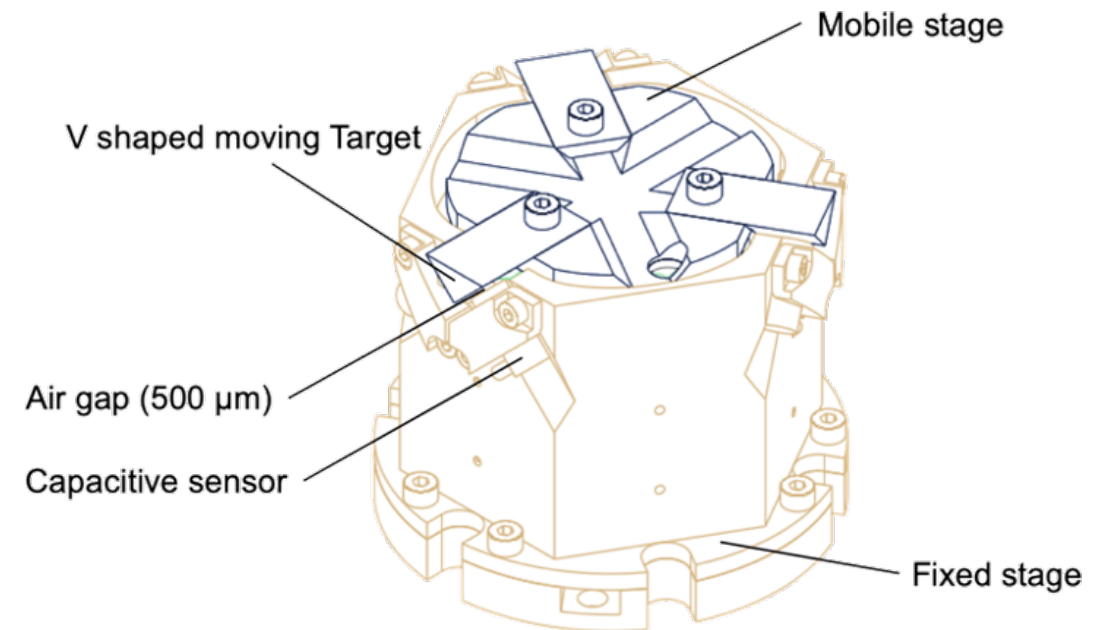
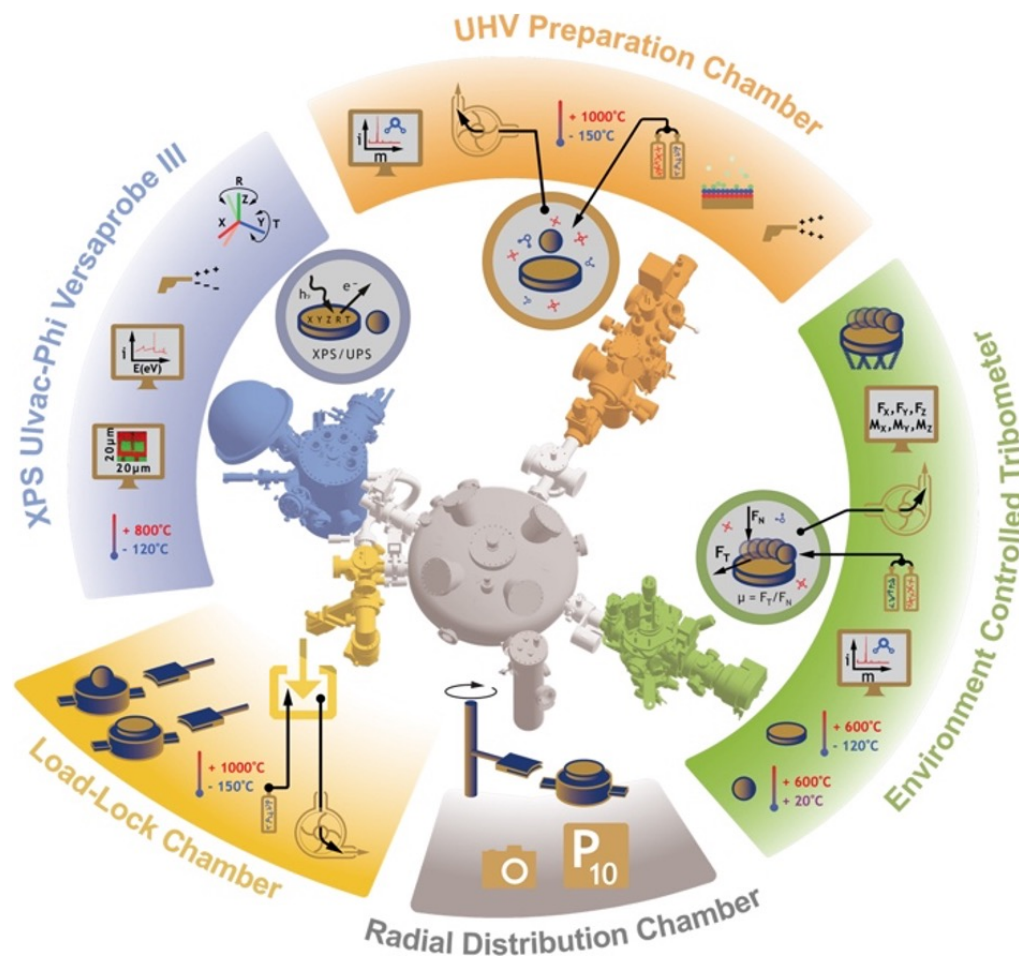
▶ **At the scale of the coating...**

- ▶ Mechanical properties control the real area of contact
- ▶ When large adhesive junctions are formed, they also control future evolution of the contact: where are these junctions released?

Few open questions on tribology of DLC...

- ▶ ***How are nanoscale adhesive junctions released?***
 - ▶ Asperities on harder **AC8** are worn much quicker than on softer **AC5**!
 - ▶ Difference in “toughness” of the asperities?
 - ▶ “Healing phenomena” thanks to time-dependant mechanical properties?
- ▶ ***What is the frequency of contact for an asperity, and its average contact time/length?***
 - ▶ This might control passivation of dangling bonds as well as “viscous” recovery of asperities...
- ▶ ***What is the critical size of adhesive junctions to have surface damage and friction increase?***
 - ▶ Is there a size effect on some kind of “ductile/brittle” transition?
 - ▶ Small junction would have plastic behavior, while large ones would lead to cracking?
- ▶ ***What is the effect of environment on mechanical behavior of asperities?***
 - ▶ If asperities are sheared, bonds should break and may react with environmental gases...

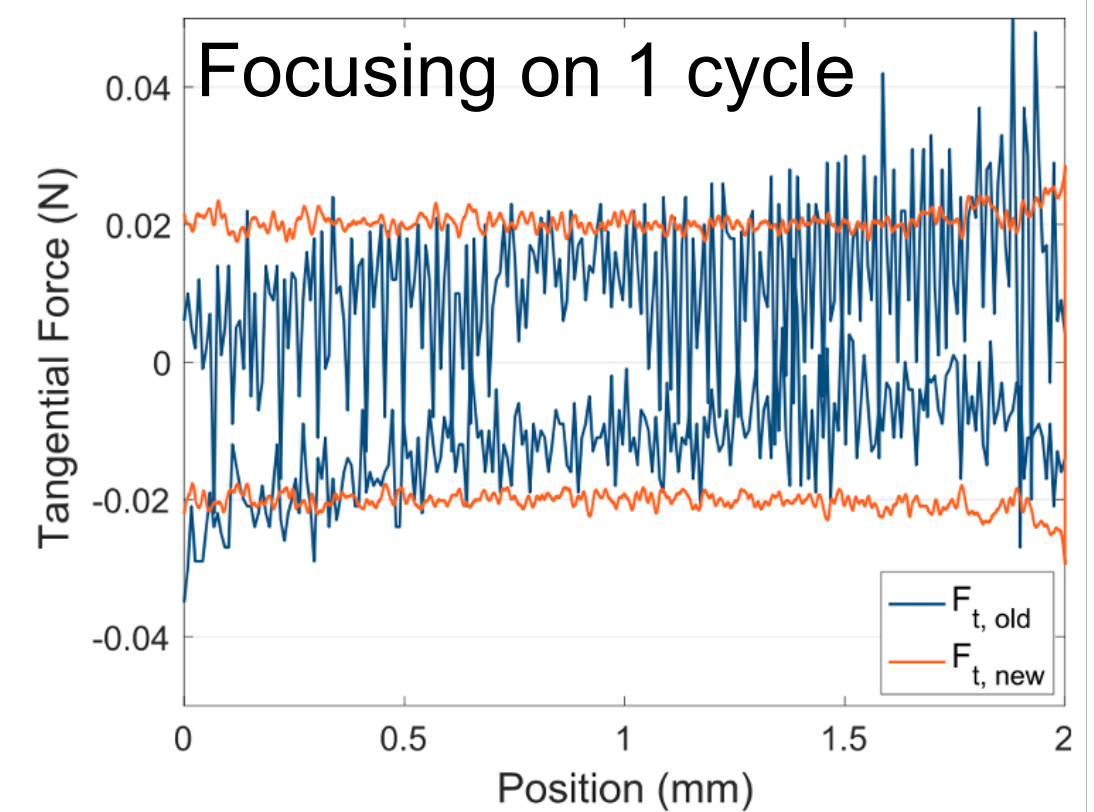
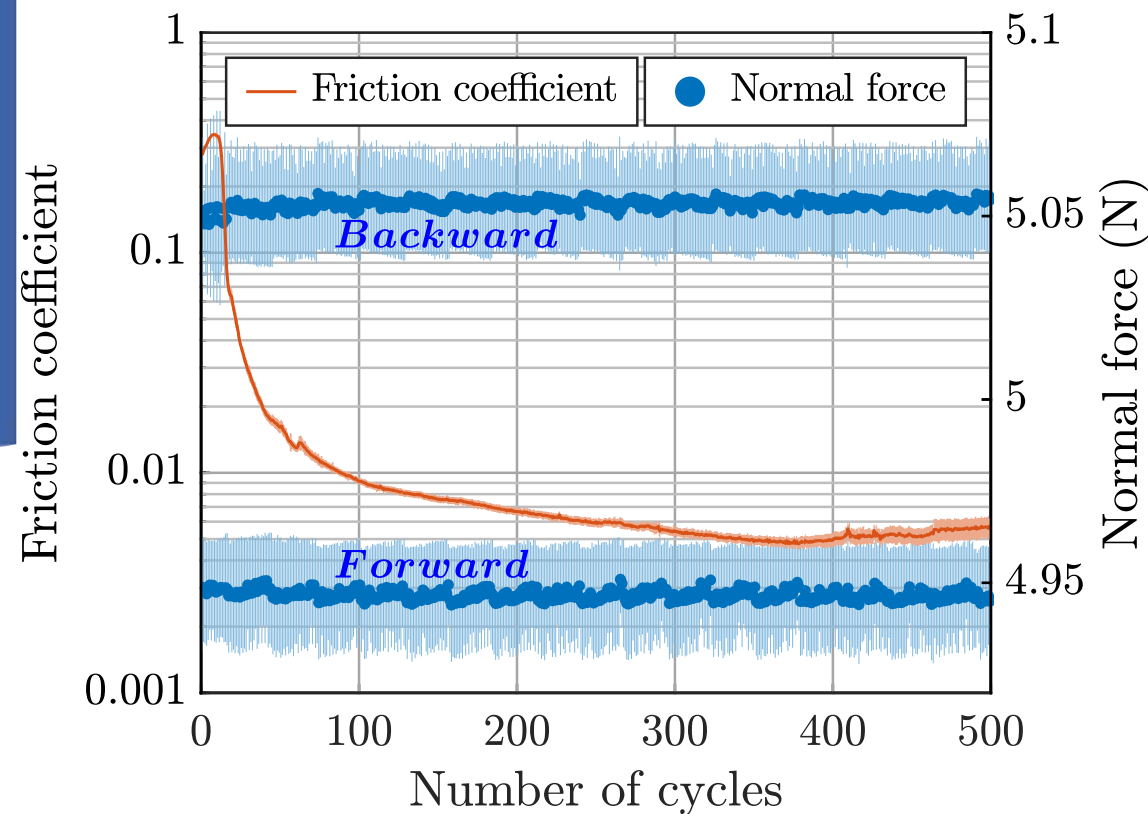
One step further in friction studies



▶ A new environment-controlled tribometer

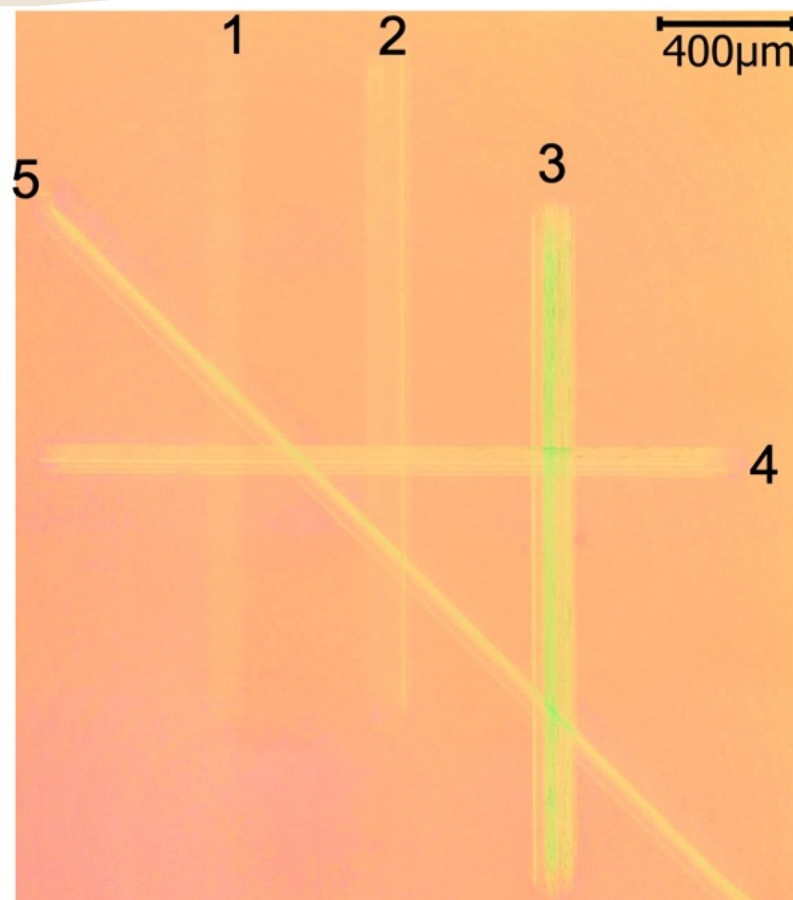
- ▶ Based on a custom 6 axes sensor
(Forces: 1 mN up to 15 N)
- ▶ 4 motion axes: X, Y, Z, R_z
- ▶ Environment: from 10⁻⁹ mBar to 1 atm
- ▶ Temperature: -120 to 600°C

One step further in friction studies

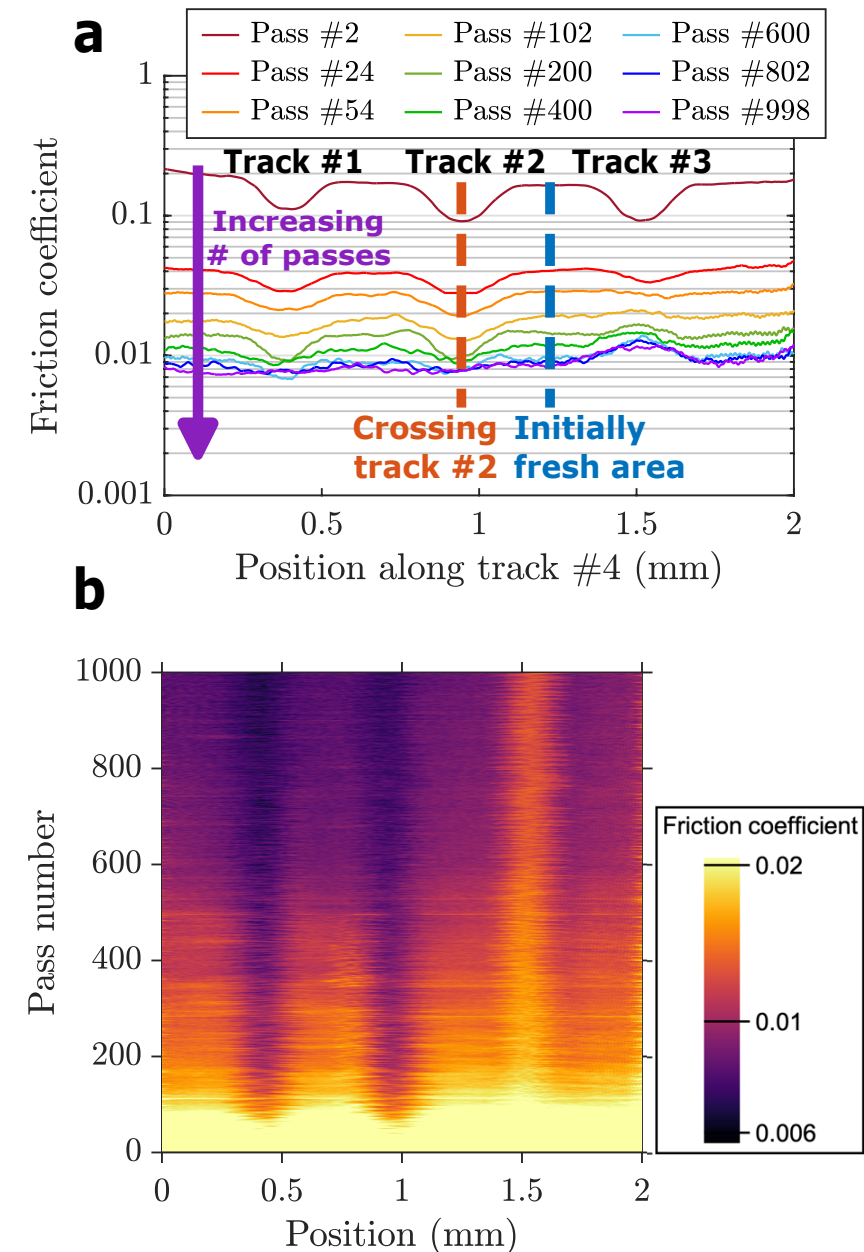


- ▶ Linear reciprocating ball-on-flat experiment
- ▶ Similar conditions as previous studies (5 N, 2 mm @ 1 mm/s...)
- ▶ Sample AC5 as in previous studies: similar results...
- ▶ **Drastic improvements in the signal/noise ratio!**

One step further in friction studies

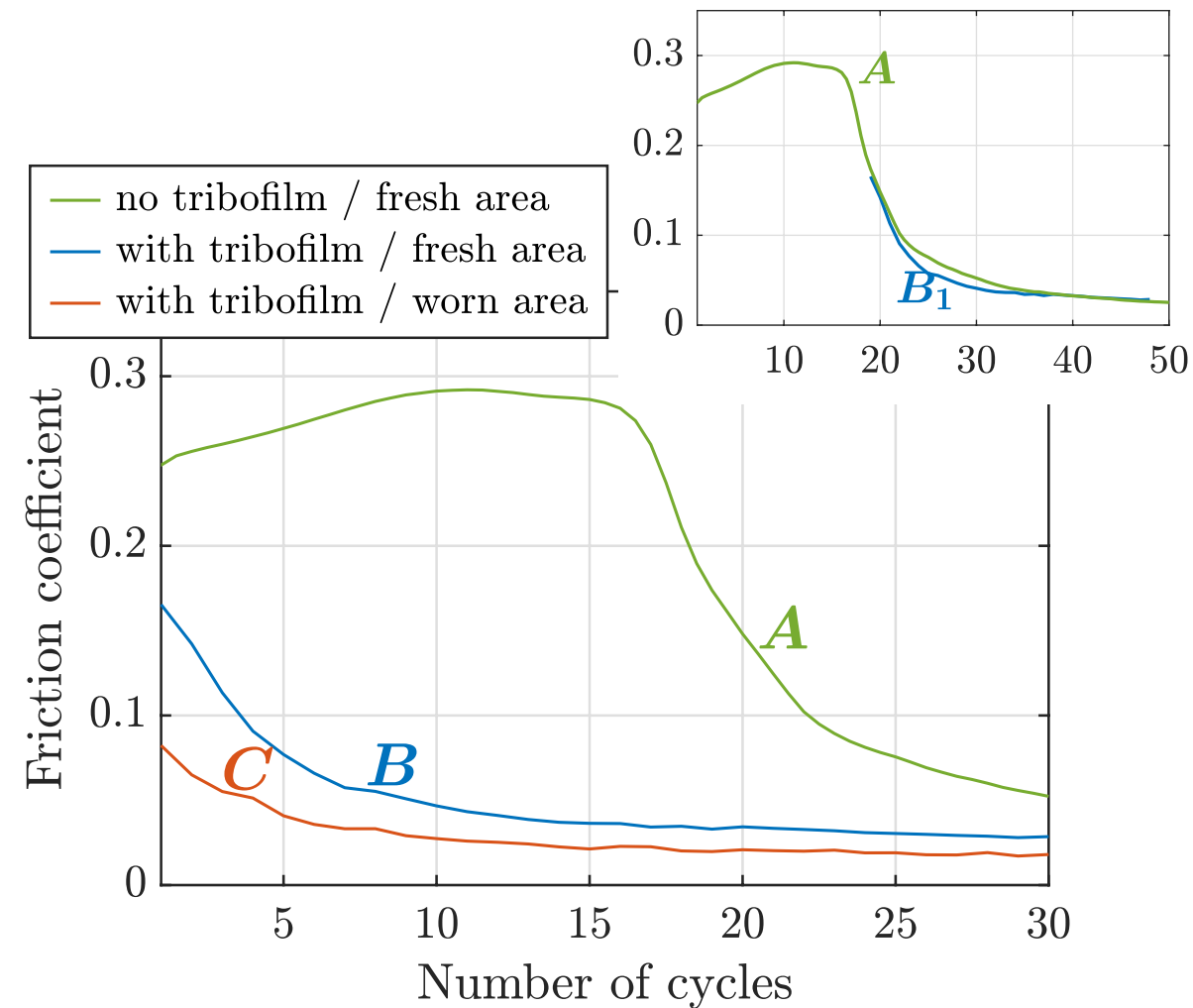


#	Initial tribofilm	Load	Length	Cycles	Orientation
1	No	3 N	2 mm	500	0°
2	Yes	5 N	2 mm	500	0°
3	Yes	5 N	2 mm	1000	0°
4	Yes	5 N	2 mm	500	90°
5	yes	5 N	3 mm	500	45°



- ▶ Crossing previous sliding tracks to probe surface modifications
- ▶ Significant friction decrease when crossing previous tracks
- ▶ It confirms that changes on the flat are necessary, friction decrease is not only due to tribofilm build-up

One step further in friction studies

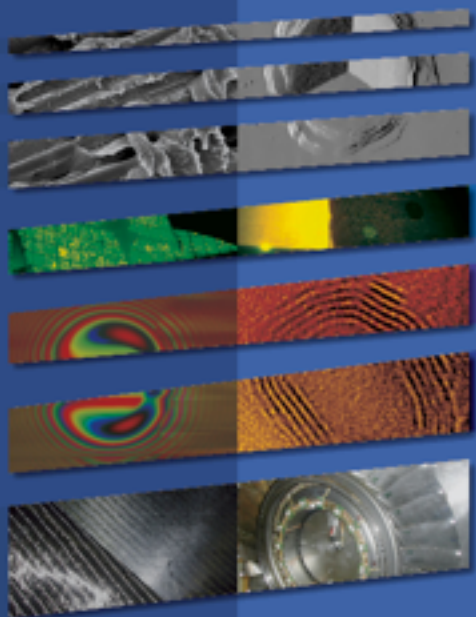


A : Friction on fresh area without previous tribofilm

B : Friction on fresh area with pre-existing tribofilm

C : Crossing of previous tracks with pre-existing tribofilm

- ▶ Pre-existing tribofilm: *initial friction reduced by 32%*
- ▶ Previous wear on the flat: *initial friction further reduced by 36%*
- ▶ Drastic shortening of the transient regime leading to low friction



Thank you for your attention!

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